## Gradually Varied Flow:

## Find Change in Depth wrt x

$$
\begin{array}{ll}
y_{1}+\frac{V_{1}^{2}}{2 g}+S_{o} \Delta x=y_{2}+\frac{V_{2}^{2}}{2 g}+S_{f} \Delta x & \begin{array}{l}
\text { Energy equation for non- } \\
\text { uniform, steady flow }
\end{array} \\
S_{o} d x=\left(y_{2}-y_{1}\right)+\left(\frac{V_{2}^{2}}{2 g}-\frac{V_{1}^{2}}{2 g}\right)+S_{f} d x & \text { Shrink control volume } \\
d y=y_{2}-y_{1} & \mathrm{~T} \\
d y+d\left(\frac{V^{2}}{2 g}\right)+S_{f} d x=S_{o} d x & \mathrm{y} \\
\frac{d y}{d y}+\frac{d}{d y}\left(\frac{V^{2}}{2 g}\right)+S_{f} \frac{d x}{d y}=S_{o} \frac{d x}{d y} & \mathrm{P}
\end{array}
$$

## Gradually Varied Flow:

## Derivative of KE wrt Depth

$$
\begin{aligned}
& \frac{d}{d y}\left(\frac{V^{2}}{2 g}\right)=\frac{d}{d y}\left(\frac{Q^{2}}{2 g A^{2}}\right)=\left(\frac{-2 Q^{2}}{2 g A^{3}}\right) \cdot \frac{d A}{d y}=\left(\frac{-Q^{2} T}{g A^{3}}\right)=-F r^{2} \\
& \frac{d y}{d y}+\frac{d}{d y}\left(\frac{V^{2}}{2 g}\right)+S_{f} \frac{d x}{d y}=S_{o} \frac{d x}{d y} \quad \quad \frac{\text { Change in KE }}{\text { Change in PE }} \quad d A=T d y \\
& \text { We are holding } \mathrm{Q} \text { constant! } \\
& 1-F r^{2}+S_{f} \frac{d x}{d y}=S_{o} \frac{d x}{d y} \\
& \text { Does } \mathrm{V}=\mathrm{Q} / \mathrm{A} \text { ? Is } \mathrm{V} \perp \mathrm{~A} \text { ? } \\
& \underline{d y}=\underline{S_{o}-S_{f}} \text { The water surface slope is a function of: } \\
& d x \quad 1-F r^{2} \quad \text { bottom slope, friction slope, Froude number }
\end{aligned}
$$

## Gradually Varied Flow: Governing equation

$\frac{d y}{d x}=\frac{S_{o}-S_{f}}{1-F r^{2}}$
Governing equation for
gradually varied flow
$>$ Gives change of water depth with distance along channel
> Note
$\Rightarrow \mathrm{S}_{\mathrm{o}}$ and $\mathrm{S}_{f}$ are positive when sloping down in direction of flow
$\Rightarrow y$ is measured from channel bottom
$>\mathrm{dy} / \mathrm{dx}=0$ means water depth is constant
$\mathbf{y}_{\mathbf{n}}$ is when $S_{o}=S_{f}$

## Surface Profiles

$\rightarrow$ Mild slope $\left(\mathrm{y}_{\mathrm{n}}>\mathrm{y}_{\mathrm{c}}\right)$
$>$ in a long channel subcritical flow will occur
$>$ Steep slope $\left(\mathrm{y}_{\mathrm{n}}<\mathrm{y}_{\mathrm{c}}\right)$
$>$ in a long channel supercritical flow will occur
$>$ Critical slope $\left(\mathrm{y}_{\mathrm{n}}=\mathrm{y}_{\mathrm{c}}\right)$
$>$ in a long channel unstable flow will occur
$>$ Horizontal slope $\left(\mathrm{S}_{\mathrm{o}}=0\right)$
$>\mathrm{y}_{\mathrm{n}}$ undefined
$>$ Adverse slope $\left(\mathrm{S}_{0}<0\right)$
$>y_{n}$ undefined
Note: These slopes are $f(Q)$ !

## Surface Profiles

## Normal depth $\vec{\rightarrow}$ <br> $\mathrm{M}_{1}$ <br> Sluice gate $\rightarrow>\rightarrow$ Mild <br> Obstruction Steep slope $\left(\mathrm{S}_{2}\right)$ Hydraulic Jump

$\frac{d y}{d x}=\frac{S_{o}-S_{f}}{1-F r^{2}}$

$$
\mathrm{S}_{0}-\mathrm{S}_{f} \quad 1-\mathrm{Fr}^{2} \quad \mathrm{dy} / \mathrm{dx}
$$

## More Surface Profiles



## Direct Step Method

$$
y_{1}+\frac{V_{1}^{2}}{2 g}+S_{o} \Delta x=y_{2}+\frac{V_{2}^{2}}{2 g}+S_{f} \Delta x \quad \text { energy equation }
$$

$$
\Delta x=\frac{y_{1}-y_{2}+\frac{V_{1}^{2}}{2 g}-\frac{V_{2}^{2}}{2 g}}{S_{f}-S_{o}} \quad \text { solve for } \Delta \mathrm{x}
$$

rectangular channel

$$
V_{1}=\frac{q}{y_{1}} \quad V_{2}=\frac{q}{y_{2}} \quad V_{2}=\frac{Q}{A_{2}} \quad V_{1}=\frac{Q}{A_{1}}
$$

## Direct Step Method Friction Slope

Manning
$S_{f}=\frac{n^{2} V^{2}}{R_{h}^{4 / 3}} \quad$ SI units
$S_{f}=\frac{n^{2} V^{2}}{2.22 R_{h}^{4 / 3}} \quad$ English units

## Darcy-Weisbach

$$
S_{f}=\mathrm{f} \frac{V^{2}}{8 g R_{h}}
$$

## Direct Step

$>$ Limitation: channel must be prismatic (channel geometry is independent of $x$ so that velocity is a function of depth only and not a function of $x$ )
$>$ Method
$>$ identify type of profile (determines whether $\Delta \mathrm{y}$ is + or -)
$\Rightarrow$ choose $\Delta \mathrm{y}$ and thus $\mathrm{y}_{\mathrm{i}+1}$
$>$ calculate hydraulic radius and velocity at $y_{i}$ and $y_{i+1}$
$>$ calculate friction slope given $\mathrm{y}_{\mathrm{i}}$ and $\mathrm{y}_{\mathrm{i}+1}$
$>$ calculate average friction slope
$>$ calculate $\Delta x$

## Direct Step Method

|  | $=y^{*}$ | $\begin{array}{r} \mathrm{b}+\mathrm{y}^{\wedge} 2 \\ =2 * \end{array}$ | $2 * z$ $y^{*}(1+$ $=\mathrm{A} / \mathrm{F}$ | z^2) | ${ }^{\wedge} 0.5+\mathrm{b}$ <br> A $=(\mathrm{n} *)$ | $)^{\wedge} 2 / \mathrm{H}$ $=y+$ | $\begin{aligned} & \Delta x \\ & h^{\wedge}(4 / 3 \\ & \left(\mathrm{V}^{\wedge} 2\right) /( \\ & =(\mathrm{G} 16 \end{aligned}$ |  | 5) | $y_{2}+$ $S_{f}$ F15+ | $S_{o}$ 16)/2 | $2 g$ <br> So) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | B | C | D | E | F | G | H | I | J | K | L | M |
| y | A | P | Rh | V | Sf | E | Dx | X | T | Fr | bottom | surface |
| 0.900 | 1.799 | 4.223 | 0.426 | 0.139 | 0.00004 | 0.901 |  | 0 | 3.799 | 0.065 | 0.000 | 0.900 |
| 0.870 | 1.687 | 4.089 | 0.412 | 0.148 | 0.00005 | 0.871 | 0.498 | 0.5 | 3.679 | 0.070 | 0.030 | 0.900 |

## Standard Step

$>$ Given a depth at one location, determine the depth at a second given location
$>$ Step size $(\Delta \mathrm{x})$ must be small enough so that changes in water depth aren't very large. Otherwise estimates of the friction slope and the velocity head are inaccurate
$>$ Can solve in upstream or downstream direction
$>$ Usually solved upstream for subcritical
$>$ Usually solved downstream for supercritical
$>$ Find a depth that satisfies the energy equation

$$
y_{1}+\frac{V_{1}^{2}}{2 g}+S_{o} \Delta x=y_{2}+\frac{V_{2}^{2}}{2 g}+S_{f} \Delta x
$$

## What curves are available? Steep Slope



Is there a curve between $y_{c}$ and $y_{n}$ that increases in depth in the downstream direction? NO!

## Mild Slope

$>$ If the slope is mild, the depth is less than the critical depth, and a hydraulic jump occurs, what happens next?

Rapidly varied flow!
When dy/dx is large then
V isn't normal to cs

Hydraulic jump! Check conjugate depths


