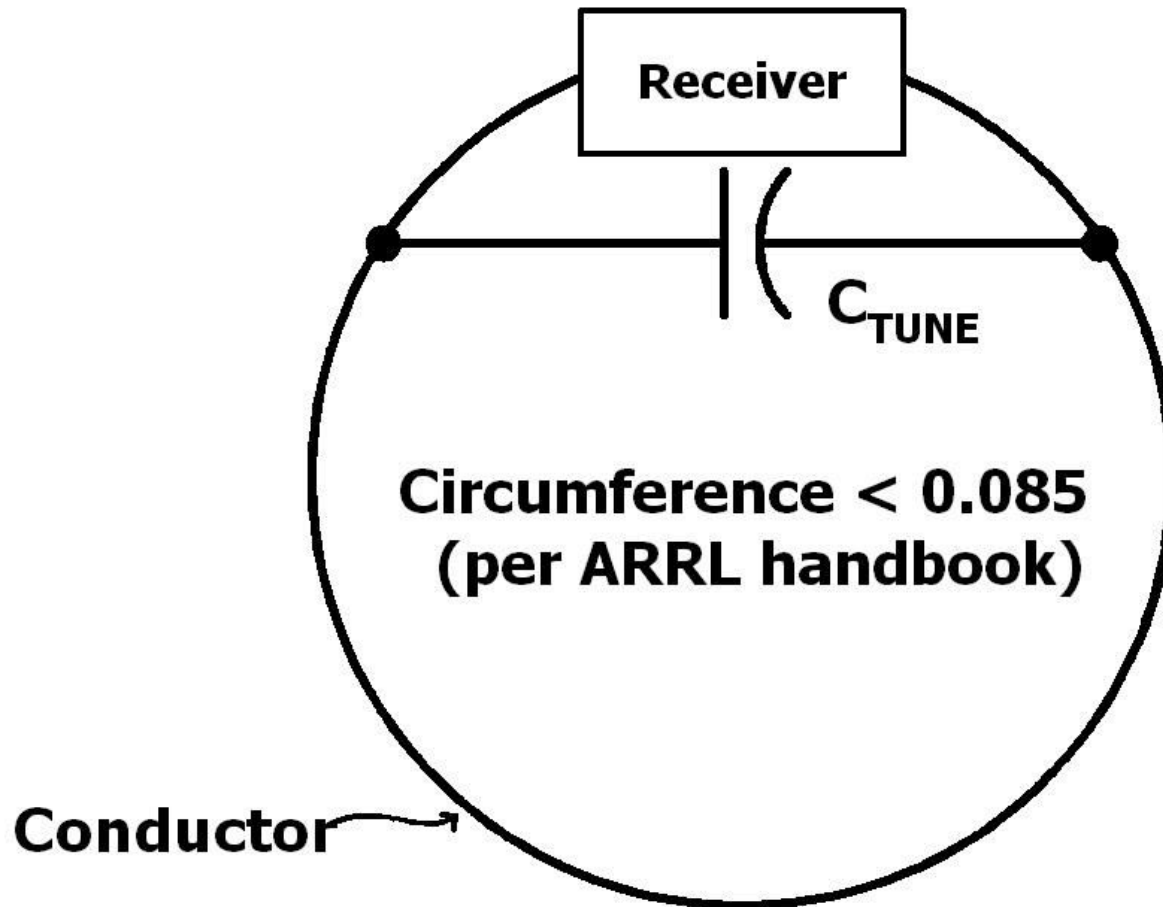




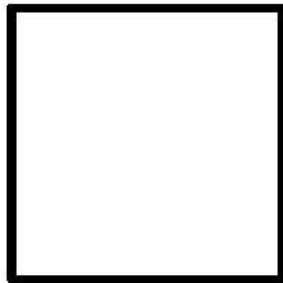
# ANTENNA AND WAVE PROPAGATION

# The classic loop antenna

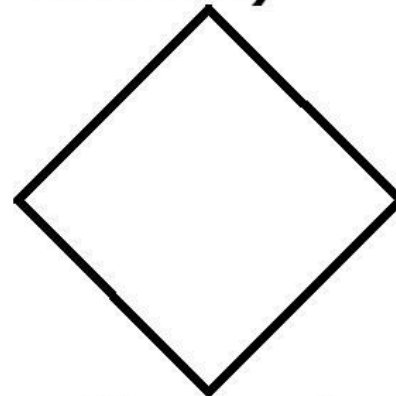


# Any symmetrical shape OK

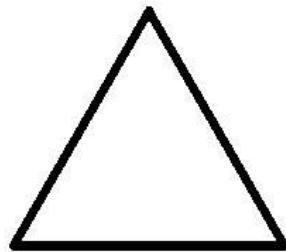
**I will discuss square loops because  
they are the simplest mechanically  
(in the form on a diamond)**



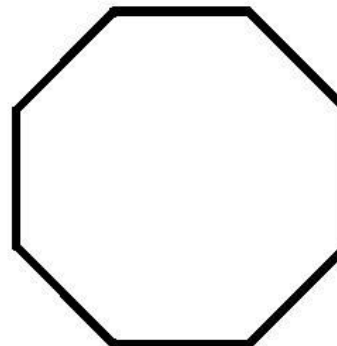
**Square**



**Diamond**



**Triangle**



**Octagon**

# Loop antenna characteristics

- Same free space pattern as a short dipole
- Directivity factor  $1.5 = 1.76$  dB
- Sharp nulls (40 to 80 dB) broadside
- Much less affected by ground and nearby objects than dipole or vertical
- Low efficiency ( $\sim 0.1$  to 1%), about the same as a modest mobile whip
- Portable (no ground radials needed)

# Why to use a receiving loop

- Can null interference (QRM or QRNN)
- Direction finding to locate QRNN
- Remote receiving antennas
- SO2R on the same band (160 meter contests, field day, SOSB, DXpeditions)
- Although vertically polarized, may be quieter than a vertical

# Design equations: size, inductance

- Maximum size side = 0.02125 wavelength
- 10 ft at 2 MHz; 5 ft at 4 MHz
- ARRL Antenna Book inductance is wrong
- $L = 0.047 s \log(1.18s/d)$
- $L = \mu\text{H}$ ;  $s = \text{side(in)}$ ;  $d = \text{conductor dia(in)}$
- Reactance of max size loop =  $226\Omega$  for  $s/d = 1000$ , independent of frequency
- Only weakly dependent on  $s/d$

# Conductor loss resistance

- We will assume copper conductor
- Conductor loss depends only on  $s/d$
- Conductor loss at 2 MHz =  $0.00047 s/d$
- If  $s/d=1000$ , conductor resistance =  $.47\Omega$
- Conductor loss at 4 MHz max size loop =  $0.00066 s/d$
- If  $s/d=1000$ , conductor resistance =  $.66\Omega$

# Radiation resistance

- Radiation resistance =  $(F_{\text{MHZ}}s/888)^4$
- For max size loop,  $R_r = 0.0064$  ohms, independent of frequency
- At 2 MHz,  $R_r = (s/444)^4$
- At 4 MHz,  $R_r = (s/222)^4$
- Radiation resistance is negligible compared to conductor loss



# Loaded $Q$ ; efficiency

- For maximum size loop,  $s/d = 1000$ , theoretical  $Q_L = 240$  @ 2 MHz, 171 @ 4 MHz
- Theoretical efficiency  $\eta = 1.4\%$  (-18.5 dB) @ 2 MHz; 0.97% (-20.1 dB) at 4 MHz
- Gain will be higher by 1.76 dB directivity factor
- Doubling  $s$  increases efficiency 9 dB
- Doubling  $d$  increases efficiency 3 dB

# Maximum circumference

- No definitive explanation of where this number comes from is published  
AFAIK
- In a “small” loop, current is uniform everywhere in loop
- As loop size increases, current phase becomes non uniform
- For large loops current magnitude is also non uniform

# Effects of “large” loop

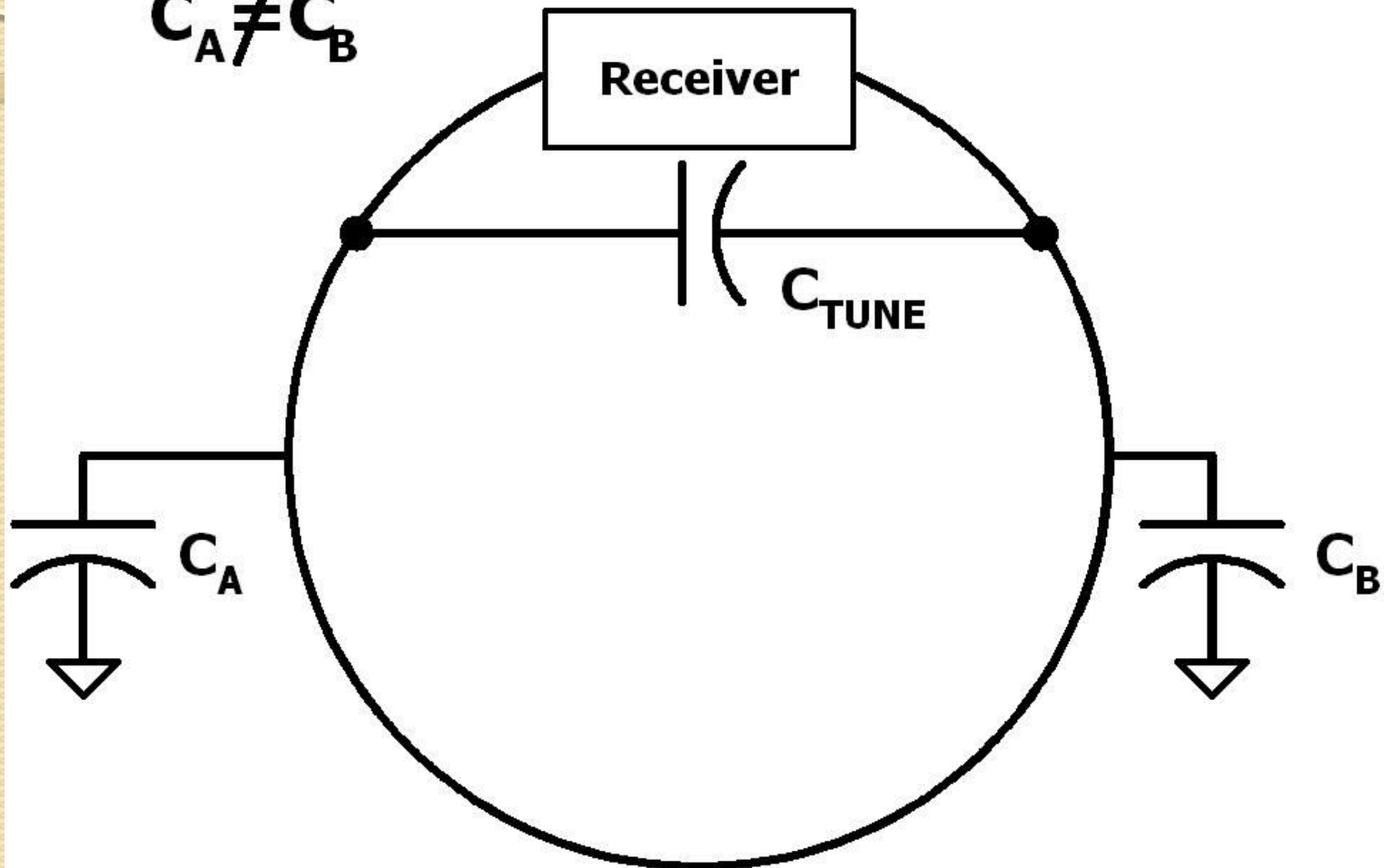
- Supposedly, a too-large loop will have poor nulls, but is this really true?
- For vertically polarized waves, there is a broadside null for any size, even a 1 wavelength “quad” driven element
- For horizontally polarized waves, there is an end fire null for any size
- Topic for further study
- I will use ARRL limit of 0.085 wavelengths

# Multiturn loops

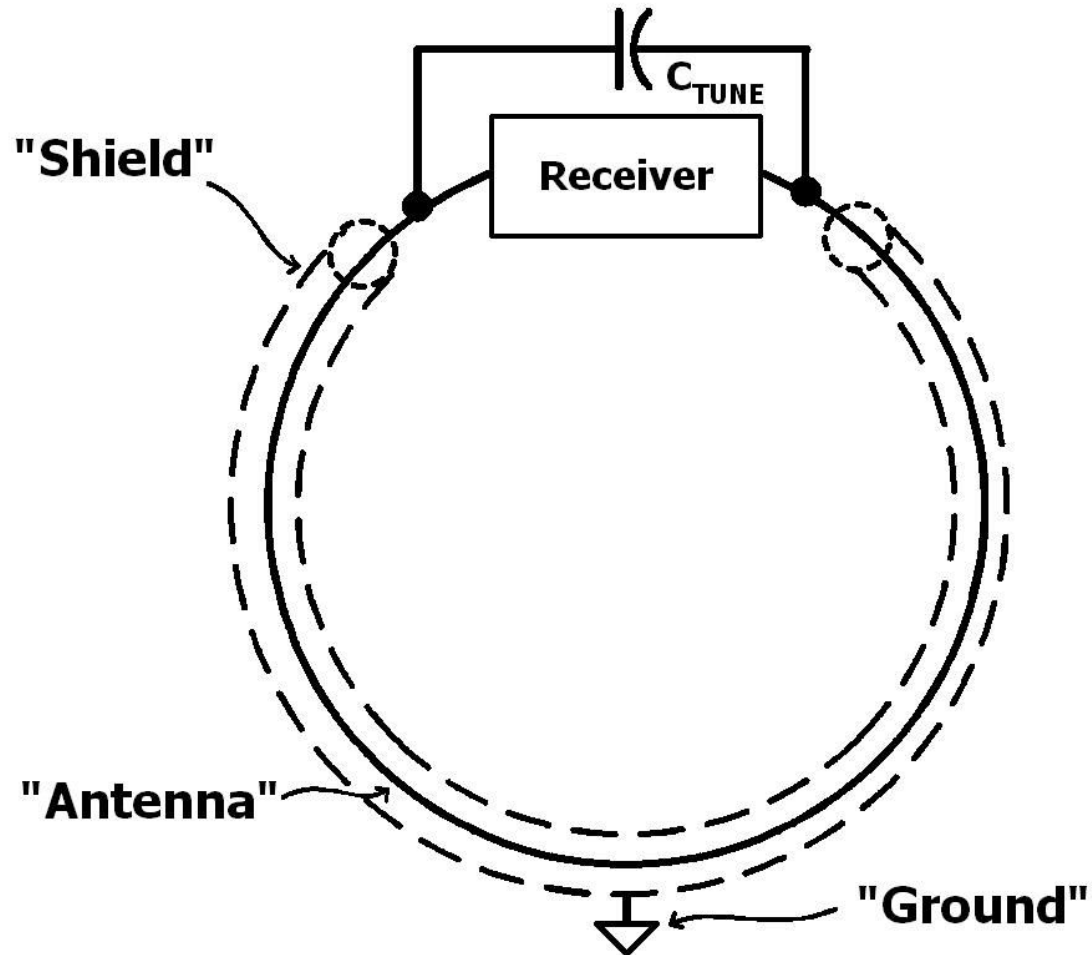
- Maximum perimeter rule applies to total length of wire, not circumference of bundle
- To the extent that max perimeter rule applies, multiturn configuration greatly limits loop size
- Multiple turns are a circuit design convenience, they do not increase loop sensitivity
- Multiple turns in parallel make more sense
- We will assume single turn from now on

# Imbalance due to stray C

$$C_A \neq C_B$$



# The classic "shielded" loop



# So-called “shielded loop”

- First described (incorrectly) in 1924 as “electrostatic shield” and repeated by Terman
- If the loop were really an electrostatic shield, we could enclose the entire loop in a shield box and it would still work; we know that is false
- Theory of shielded loop as published overlooks skin effect
- Shielded loop actually works and is useful, but not for the reasons given in handbooks

# Disproof of electrostatic shield

