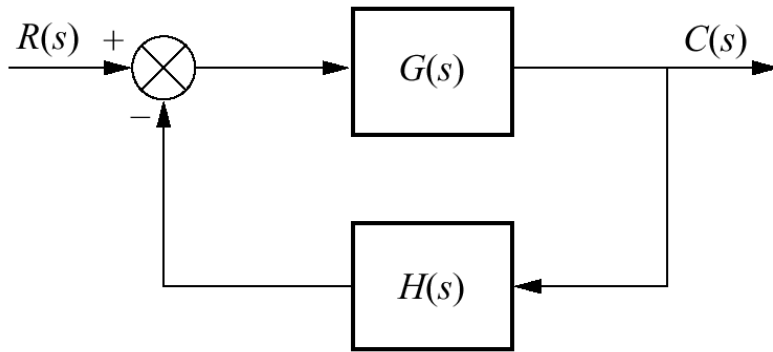


# Frequency Response Method

# Knowledge Before Studying Nyquist Criterion



$$T(s) = \frac{G(s)}{1 + G(s)H(s)}$$

**unstable if there is any pole on RHP (right half plane)**

$$G(s) = \frac{N_G(s)}{D_G(s)}$$

$$H(s) = \frac{N_H(s)}{D_H(s)}$$

**Open-loop system:**

$$G(s)H(s) = \frac{N_G(s) N_H(s)}{D_G(s) D_H(s)}$$

**Characteristic equation:**

$$1 + G(s)H(s) = 1 + \frac{N_G N_H}{D_G D_H} = \frac{D_G D_H + N_G N_H}{D_G D_H}$$

**poles of  $G(s)H(s)$  and  $1+G(s)H(s)$  are the same**

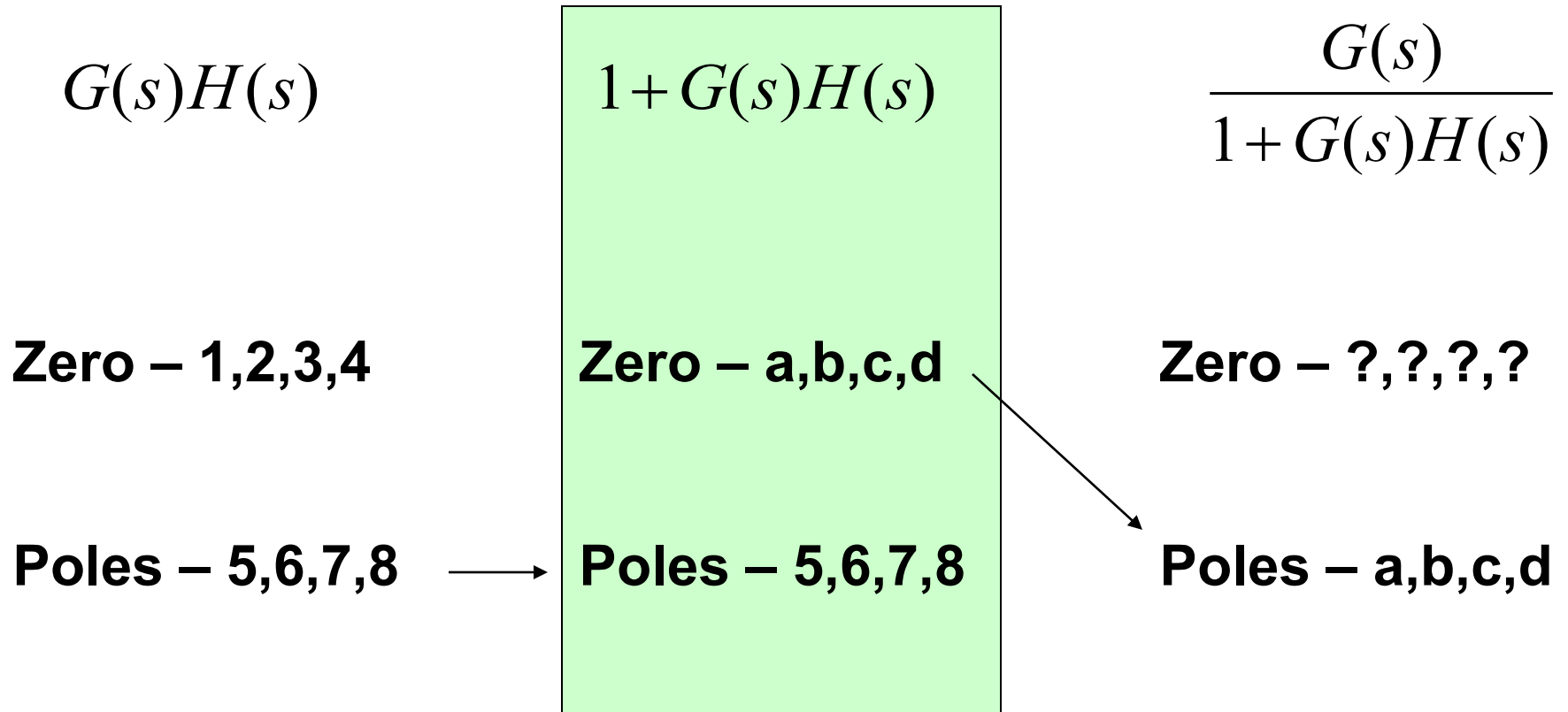
**Closed-loop system:**

$$T(s) = \frac{G(s)}{1 + G(s)H(s)} = \frac{N_G(s)D_H(s)}{D_G(s)D_H(s) + N_G(s)N_H(s)}$$

**zero of  $1+G(s)H(s)$  is pole of  $T(s)$**

$$G(s)H(s) = \frac{(s-1)(s-2)(s-3)(s-4)}{(s-5)(s-6)(s-7)(s-8)}$$


---



**To know stability, we have to know a,b,c,d**

# Stability from Nyquist plot

**From a Nyquist plot, we can tell a number of closed-loop poles on the right half plane.**

- If there is any closed-loop pole on the right half plane, the system goes unstable.**
- If there is no closed-loop pole on the right half plane, the system is stable.**

# Nyquist Criterion

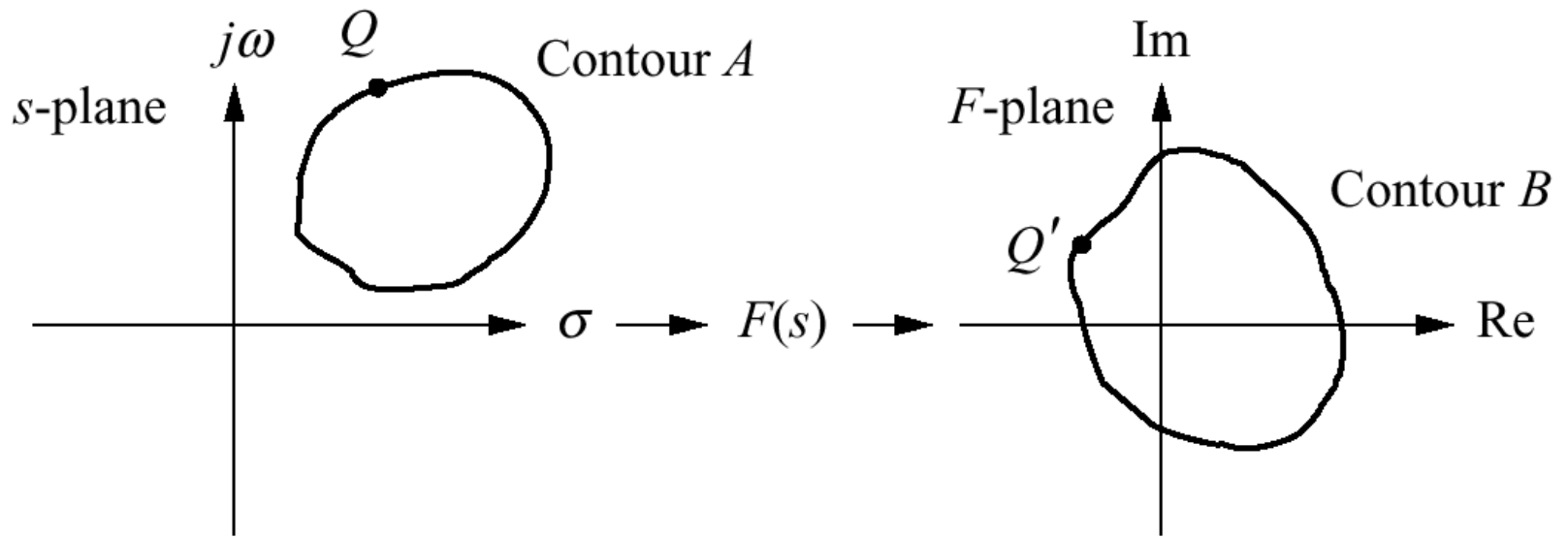
**Nyquist plot is a plot used to verify stability of the system.**

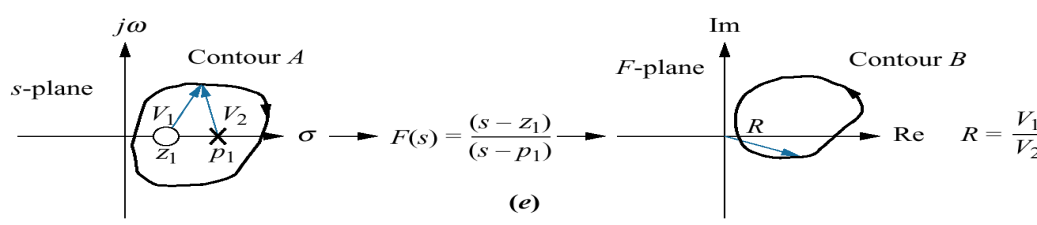
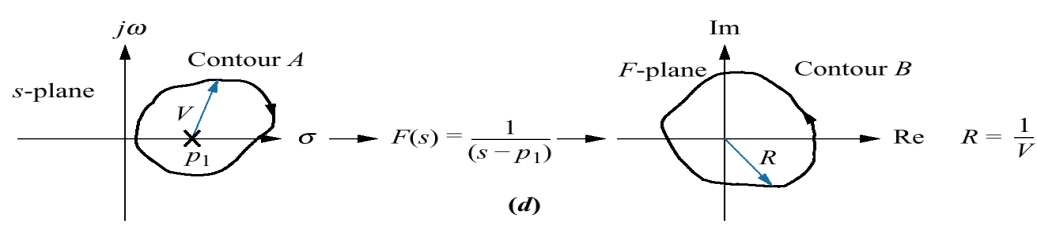
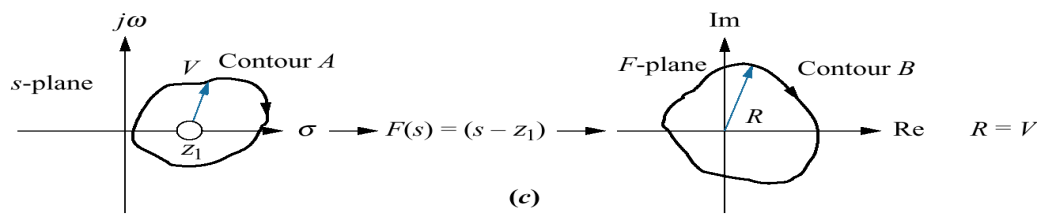
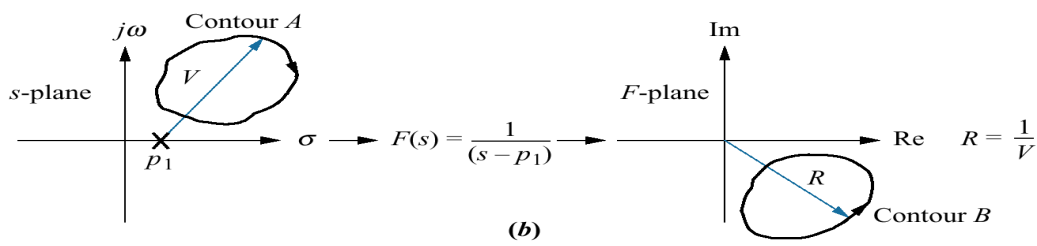
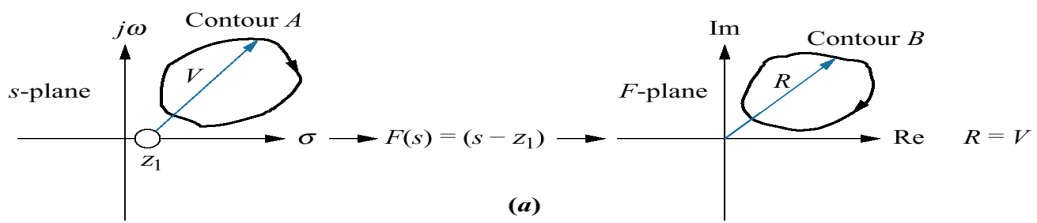
**mapping contour**

**function** 
$$F(s) = \frac{(s - z_1)(s - z_2)}{(s - p_1)(s - p_2)}$$

**mapping all points (contour) from one plane to another by function F(s).**

$$F(s) = \frac{(s - z_1)(s - z_2)}{(s - p_1)(s - p_2)}$$



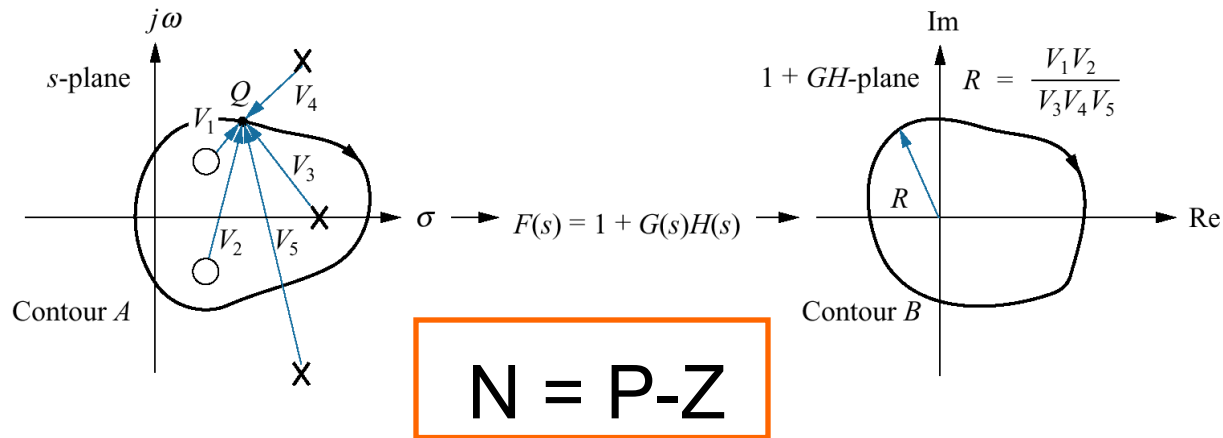


- Pole/zero inside the contour has 360 deg. angular change.
- Pole/zero outside contour has 0 deg. angular change.
- Move clockwise around contour, zero inside yields rotation in clockwise, pole inside yields rotation in counterclockwise



# Characteristic equation

$$F(s) = 1 + G(s)H(s)$$



$N$  = # of counterclockwise direction about the origin

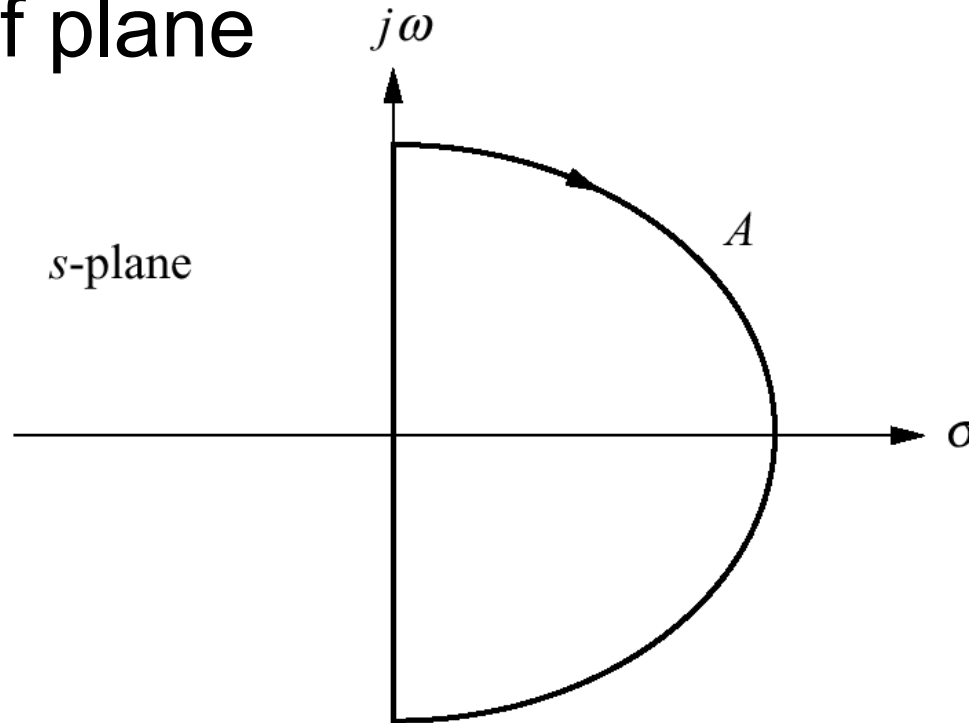
$P$  = # of poles of characteristic equation inside contour  
= # of poles of open-loop system

$Z$  = # of zeros of characteristic equation inside contour  
= # of poles of closed-loop system

$$Z = P - N$$

# Characteristic equation

- Increase size of the contour to cover the right half plane



- More convenient to consider the open-loop system (with known pole/zero)

# Nyquist diagram of $G(s)H(s)$

‘Open-loop system’

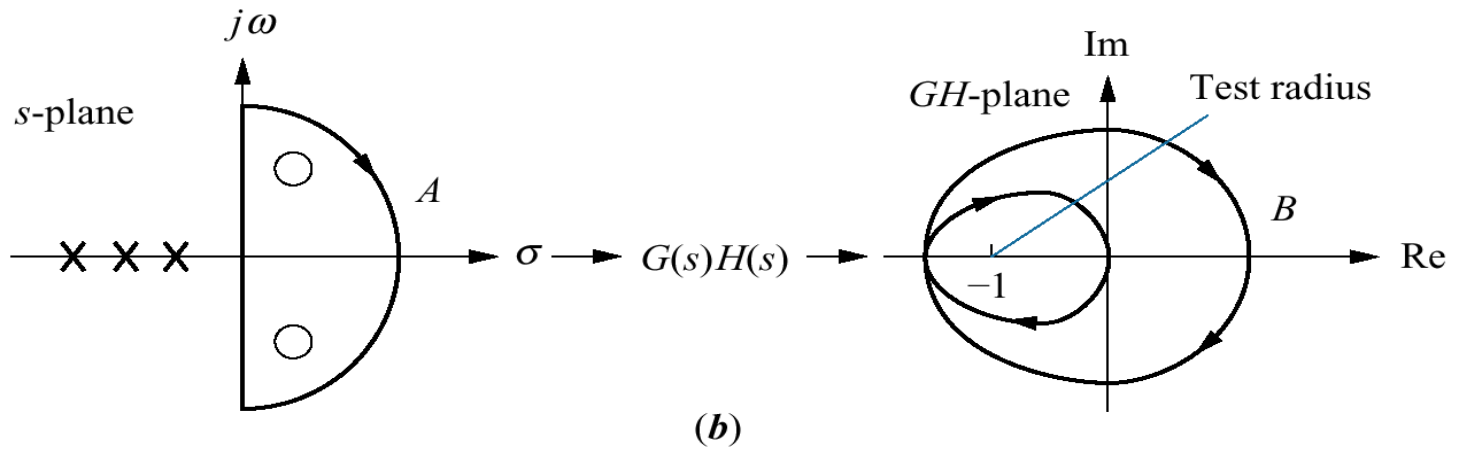
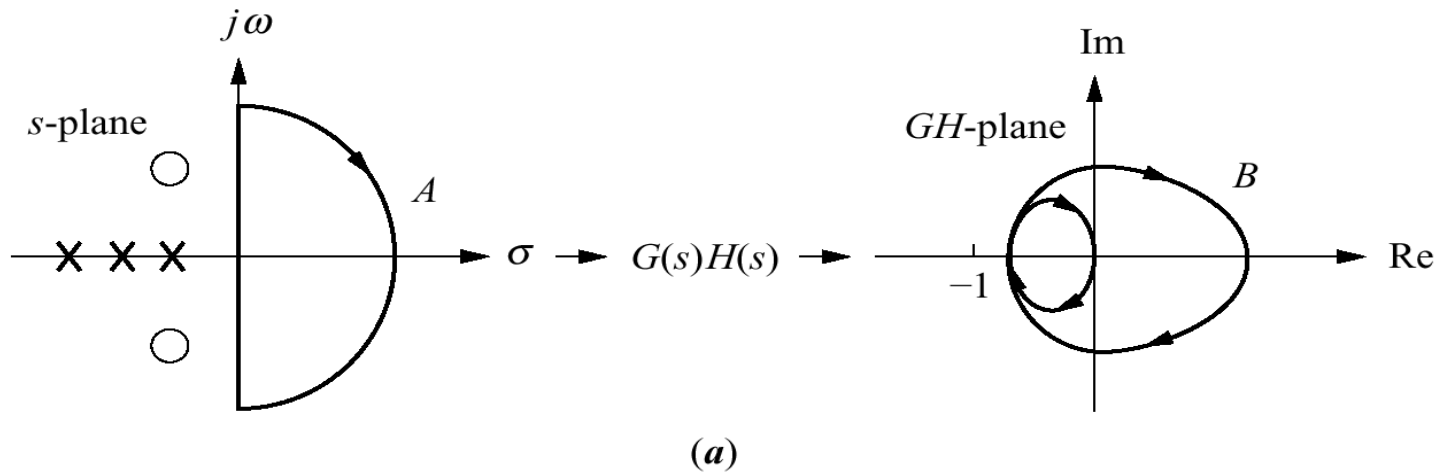
Mapping from characteristic equ. to open-loop system by shifting to the left one step

$$Z = P - N$$

Z = # of closed-loop poles inside the right half plane

P = # of open-loop poles inside the right half plane

N = # of counterclockwise revolutions around -1

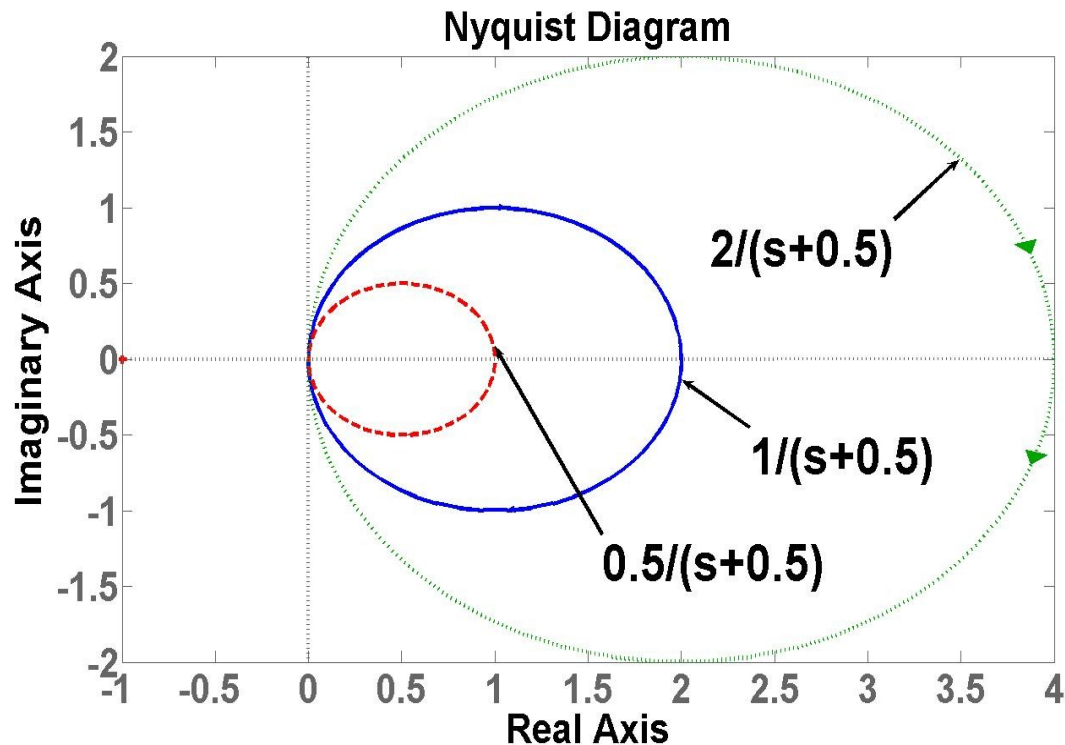


$\circ$  = zeros of  $1 + G(s)H(s)$   
 = poles of closed-loop system  
 Location not known

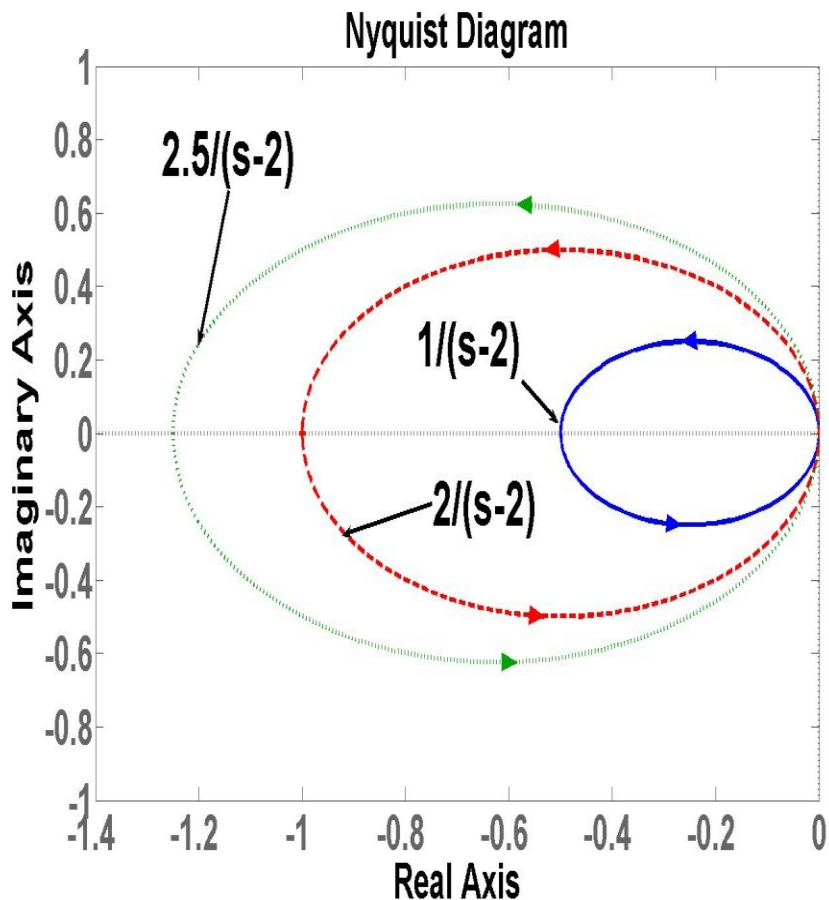
$\times$  = poles of  $1 + G(s)H(s)$   
 = poles of  $G(s)H(s)$   
 Location is known

# Properties of Nyquist plot

If there is a gain,  $K$ , in front of open-loop transfer function, the Nyquist plot will expand by a factor of  $K$ .



# Nyquist plot example



- Open loop system has pole at 2

$$G(s) = \frac{1}{s-2}$$

- Closed-loop system has pole at 1

$$\frac{G(s)}{1+G(s)} = \frac{1}{(s-1)}$$

- If we multiply the open-loop with a gain,  $K$ , then we can move the closed-loop pole's position to the left-half plane

# Nyquist plot example (cont.)

- New look of open-loop system:

$$G(s) = \frac{K}{s-2}$$

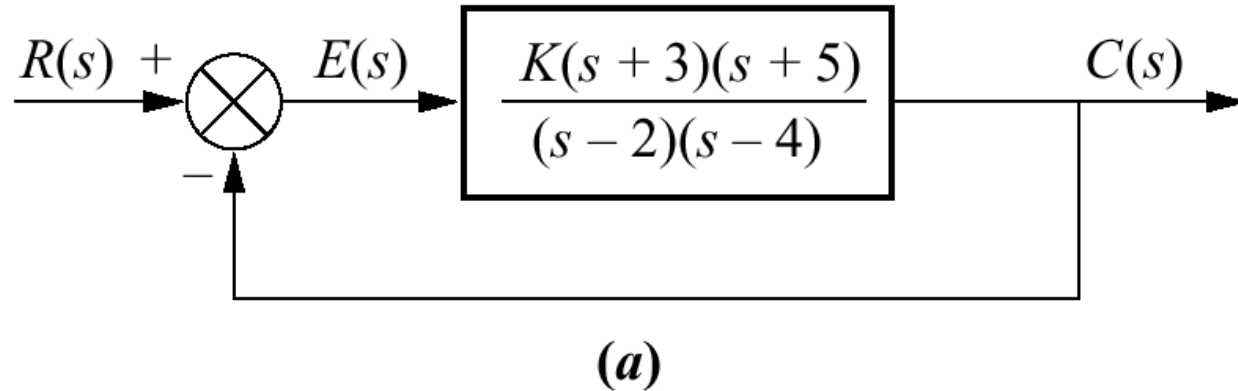
- Corresponding closed-loop system:

$$\frac{G(s)}{1+G(s)} = \frac{K}{s+(K-2)}$$

- Evaluate value of K for stability

$$K \geq 2$$

# Adjusting an open-loop gain to guarantee stability



**Step I:** sketch a Nyquist Diagram

**Step II:** find a range of  $K$  that makes the system stable!



# How to make a Nyquist plot?

Easy way by Matlab

- Nyquist: 'nyquist'
- Bode: 'bode'

# Step I: make a Nyquist plot

- Starts from an open-loop transfer function (set  $K=1$ )
- Set  $s = j\omega$  and find frequency response
  - At dc,  $\omega = 0 \rightarrow s = 0$
  - **Find  $\omega$  at which the imaginary part equals zero**

$$G(s)H(s) = \frac{(s+3)(s+5)}{(s-2)(s-4)} = \frac{s^2 + 8s + 15}{s^2 - 6s + 8}$$

$$G(j\omega)H(j\omega) = \frac{-\omega^2 + 8j\omega + 15}{-\omega^2 - 6j\omega + 8} = \frac{(15 - \omega^2) + 8j\omega}{(8 - \omega^2) - 6j\omega}$$

$$= \frac{(15 - \omega^2) + 8j\omega}{(8 - \omega^2) - 6j\omega} \times \frac{(8 - \omega^2) + 6j\omega}{(8 - \omega^2) + 6j\omega}$$

$$= \frac{(15 - \omega^2)(8 - \omega^2) - 48\omega^2 + j(154\omega - 14\omega^3)}{(8 - \omega^2)^2 + 6^2\omega^2}$$

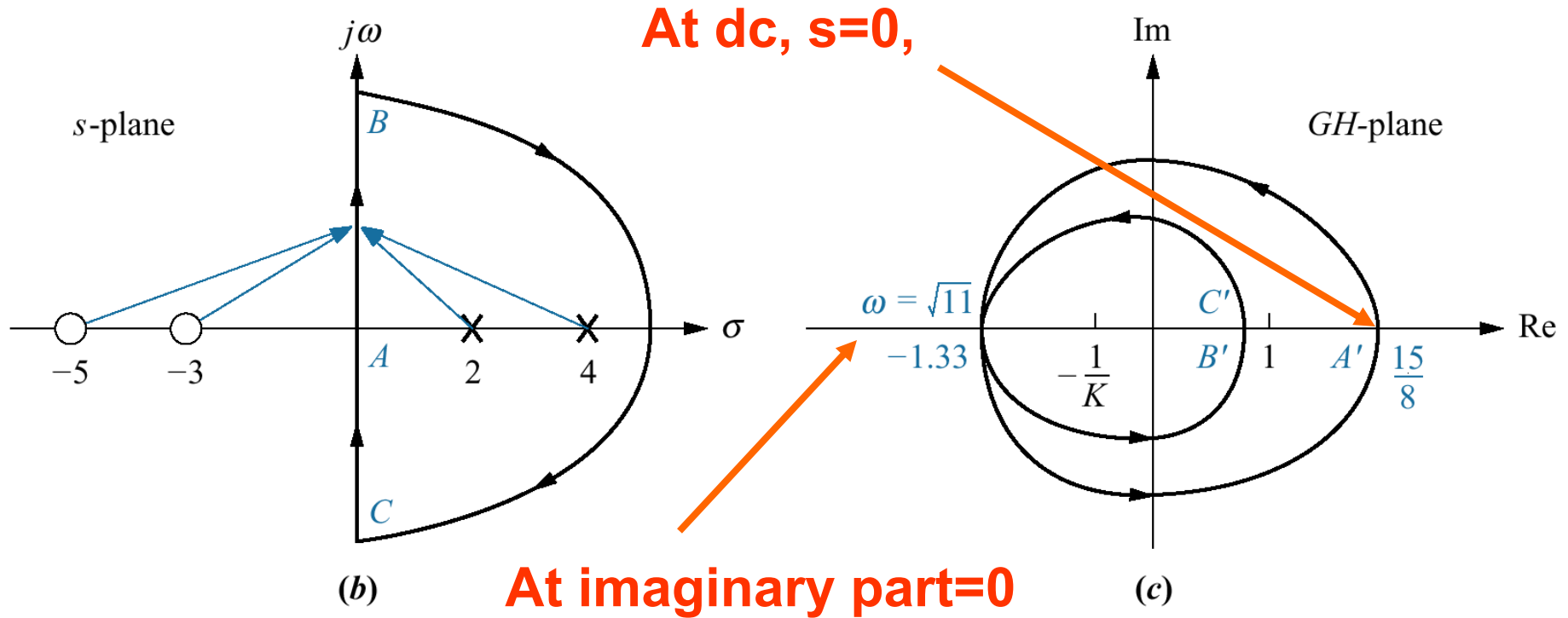
$$\omega = 0, \sqrt{11}$$

**Need the imaginary term = 0,**

**Substitute  $\omega = \sqrt{11}$  back in to the transfer function**

**And get  $G(s) = -1.33$**

$$\frac{(15-11)(8-11) - 48(11)}{(8-11)^2 + 6^2(11)} = \frac{-540}{412} = -1.31$$



## Step II: satisfying stability condition

- **P = 2, N has to be 2 to guarantee stability**
- **Marginally stable if the plot intersects -1**
- **For stability, 1.33K has to be greater than 1**

$$K > 1/1.33$$

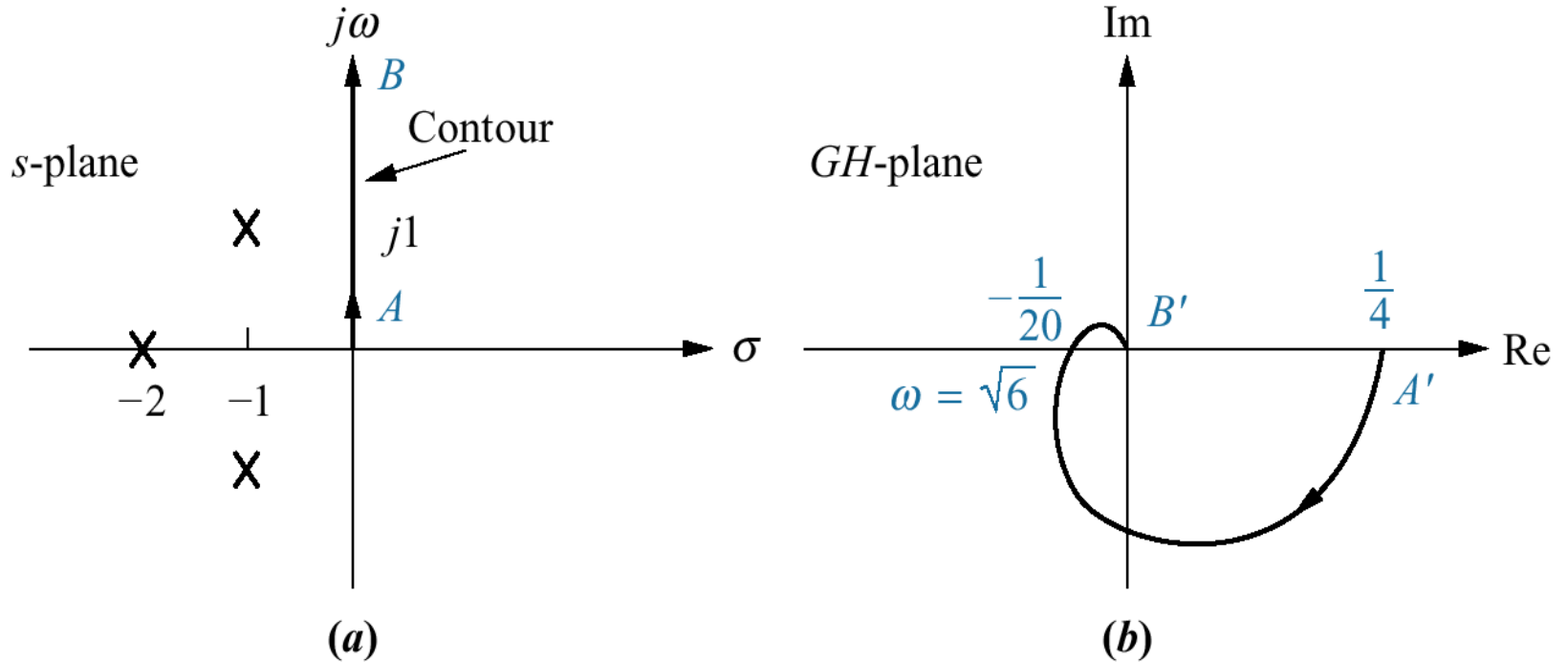
or

$$K > 0.75$$

# Example

Evaluate a range of  $K$  that makes the system stable

$$G(s) = \frac{K}{(s^2 + 2s + 2)(s + 2)}$$



Step I: find frequency at which imaginary part = 0

**Set  $s = j\omega$**

$$G(j\omega) = \frac{K}{((j\omega)^2 + 2j\omega + 2)(j\omega + 2)}$$
$$= \frac{4(1 - \omega^2) - j\omega(6 - \omega^2)}{16(1 - \omega^2)^2 + \omega^2(6 - \omega^2)^2}$$

**At  $\omega = 0, \sqrt{6}$  the imaginary part = 0**

**Plug  $\omega = \sqrt{6}$  back in the transfer function  
and get  $G = -0.05$**

# Step II: consider stability condition

- **$P = 0$ ,  $N$  has to be  $0$  to guarantee stability**
- **Marginally stable if the plot intersects  $-1$**
- **For stability,  $0.05K$  has to be less than  $1$**

$$K < 1/0.05$$

or

$$K < 20$$



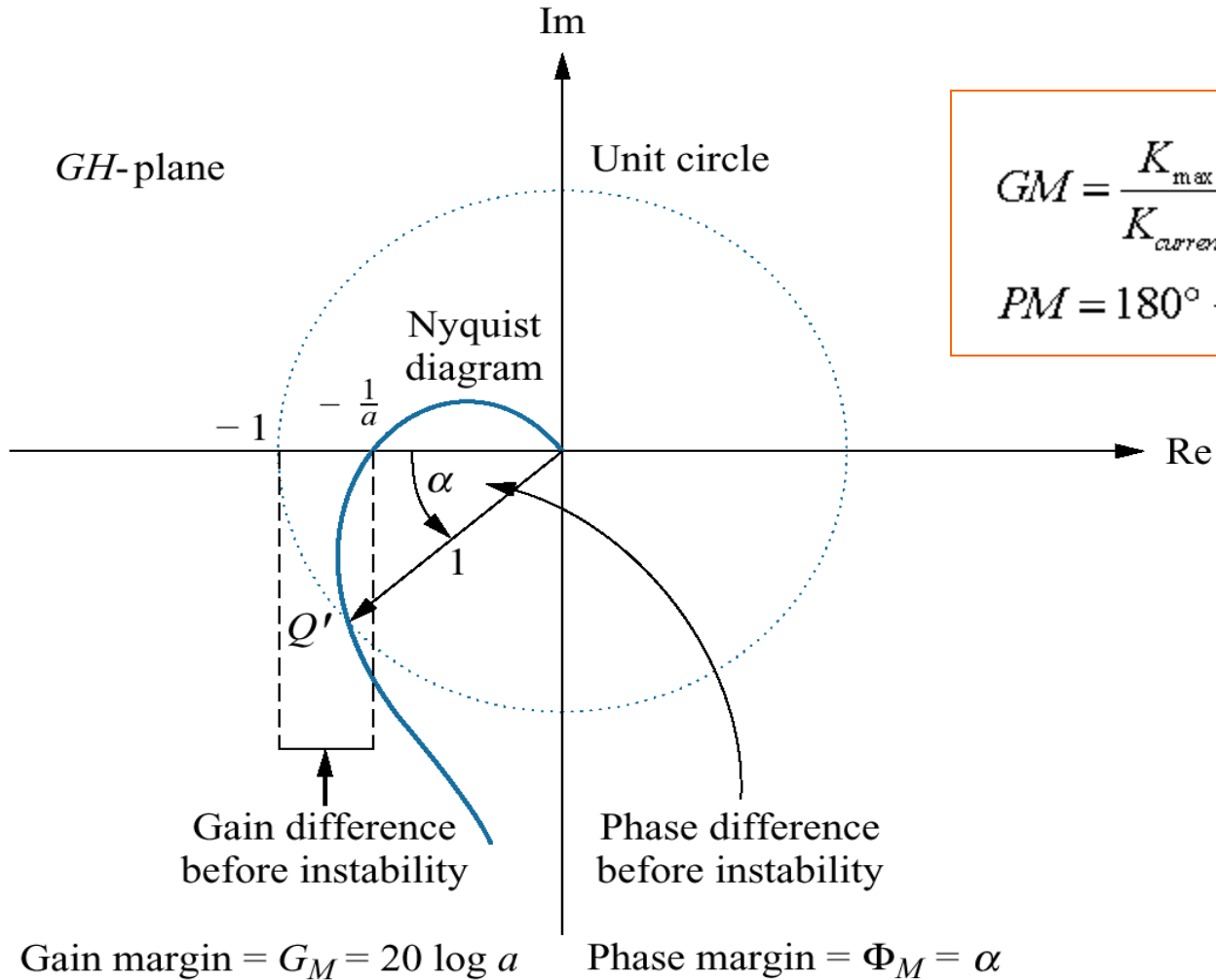
# Gain Margin and Phase Margin

**Gain margin is the change in open-loop gain (in dB), required at 180 of phase shift to make the closed-loop system unstable.**

**Phase margin is the change in open-loop phase shift, required at unity gain to make the closed-loop system unstable.**

**GM/PM tells how much system can tolerate before going unstable!!!**

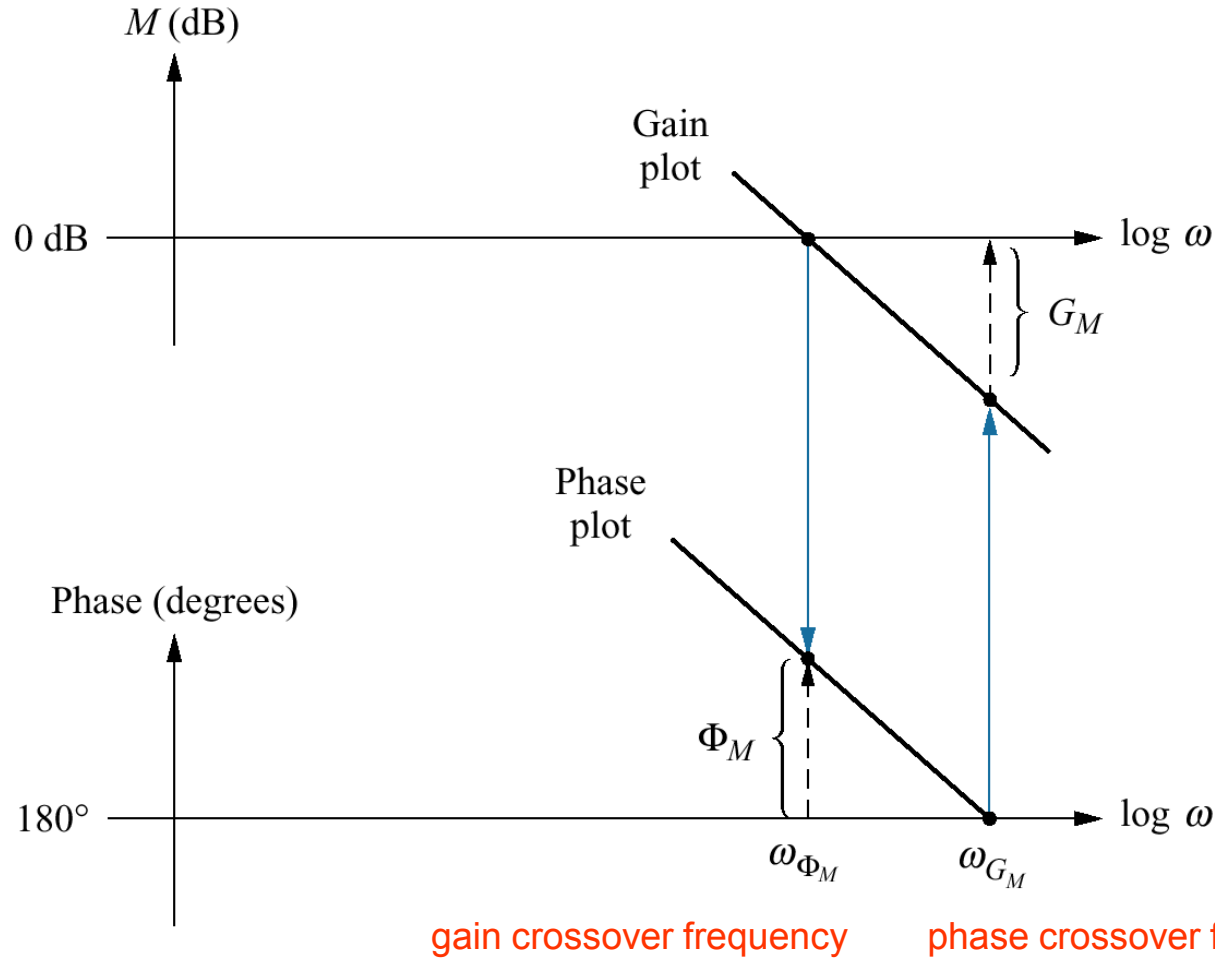
# GM and PM via Nyquist plot



$$GM = \frac{K_{\max}}{K_{\text{current}}} = \frac{1}{|G(j\omega_\phi)H(j\omega_\phi)|}$$

$$PM = 180^\circ + \angle G(j\omega_x)H(j\omega_x)$$

# GM and PM via Bode Plot



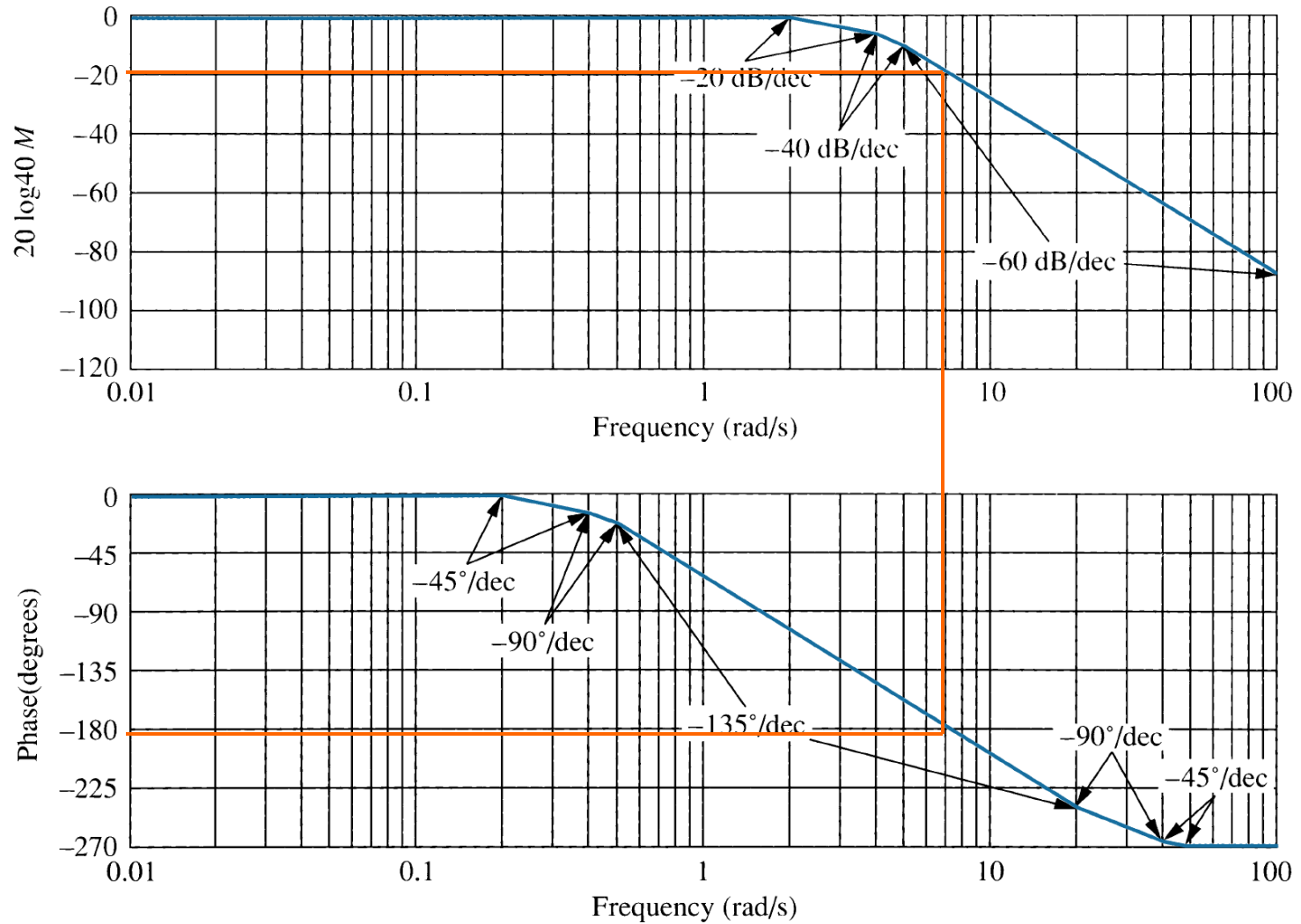
- The frequency at which the phase equals  $180^\circ$  is called the phase crossover frequency  $\omega_{G_M}$
- The frequency at which the magnitude equals 1 is called the gain crossover frequency  $\omega_{\Phi_M}$

# Example

**Find Bode Plot and evaluate a value of K that makes the system stable  
The system has a unity feedback with an open-loop transfer function**

$$G(s) = \frac{K}{(s + 2)(s + 4)(s + 5)}$$

**First, let's find Bode Plot of G(s) by assuming that K=40 (the value at which magnitude plot starts from 0 dB)**

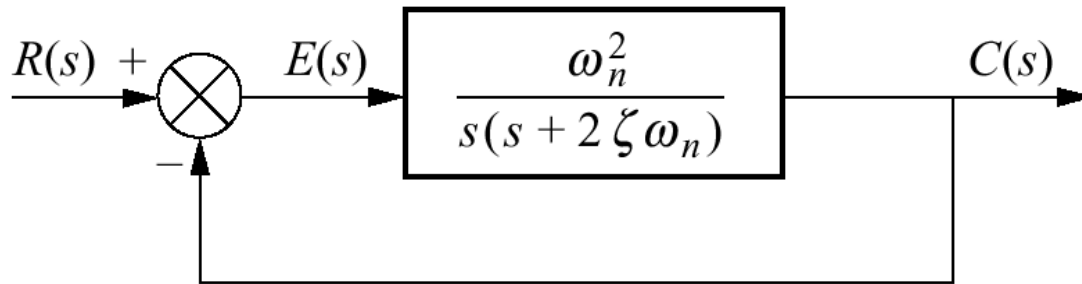


**At phase = -180,  $\omega = 7$  rad/sec, magnitude = -20 dB**

- **GM>0, system is stable!!!**
- **Can increase gain up 20 dB without causing instability (20dB = 10)**
- **Start from K = 40**
- **with K < 400, system is stable**

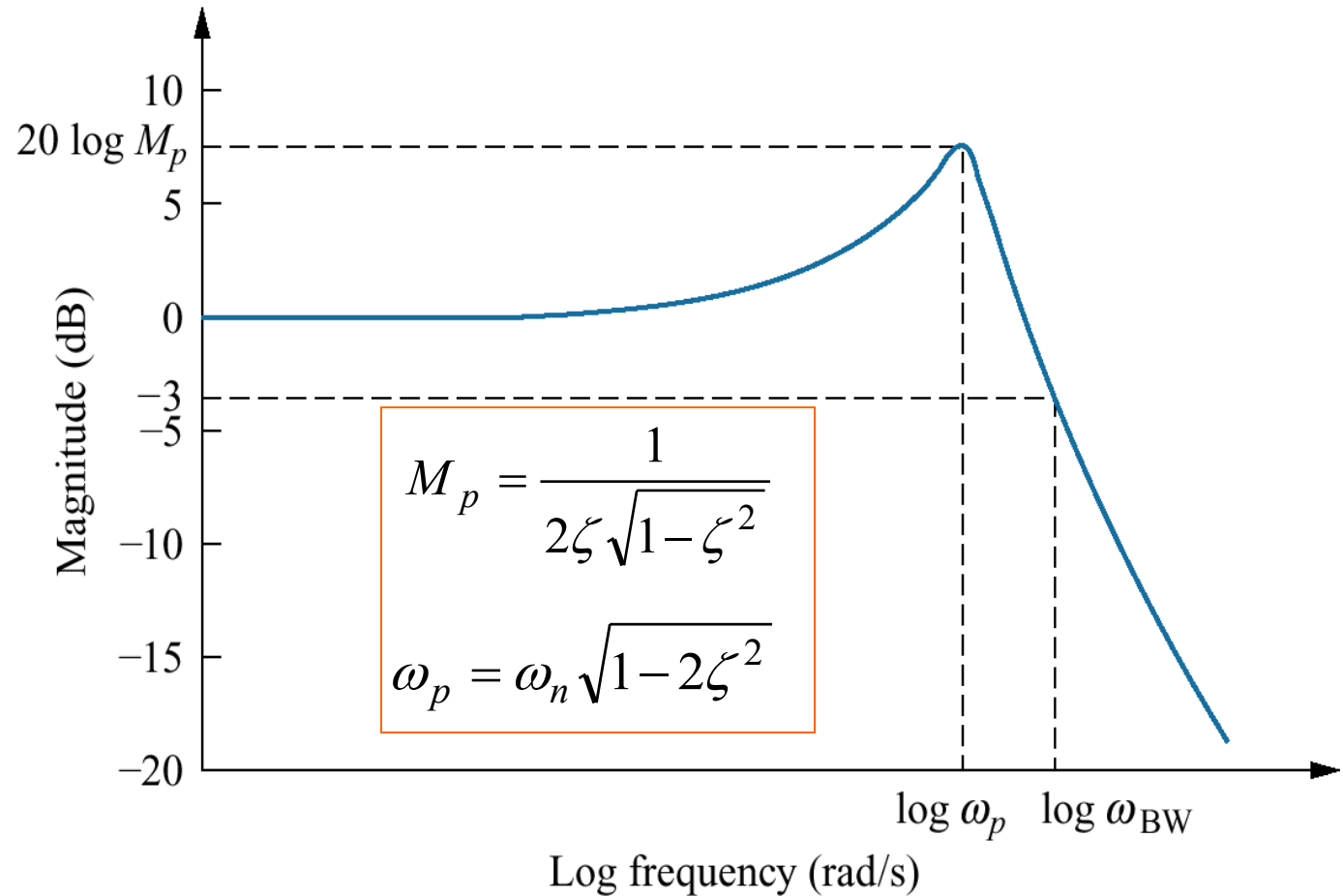
# Closed-loop transient and closed-loop frequency responses

## '2<sup>nd</sup> system'



$$\frac{C(s)}{R(s)} = T(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

# Damping ratio and closed-loop frequency response



**Magnitude Plot of closed-loop system**



## Response speed and closed-loop frequency response

$$\omega_{BW} = \omega_n \sqrt{(1-2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2 + 2}}$$

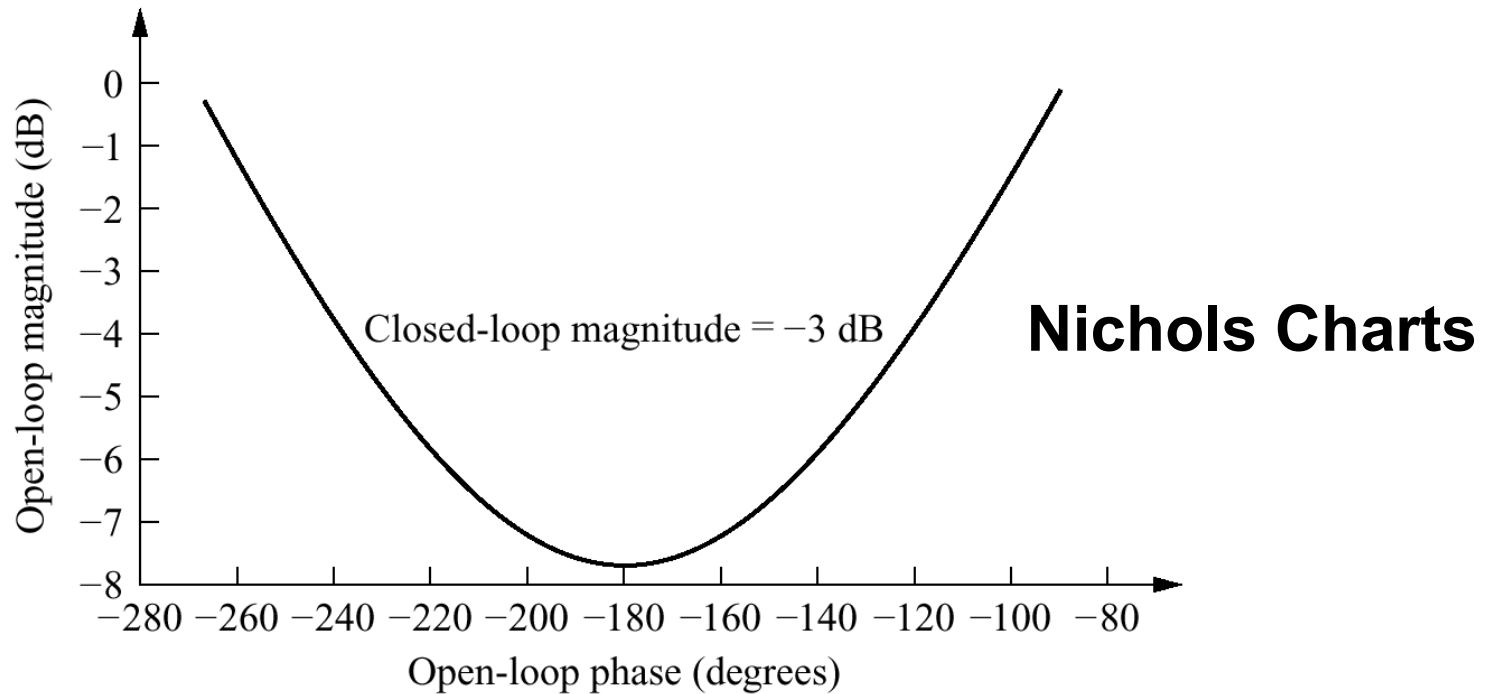
$$\omega_{BW} = \frac{4}{T_s \zeta} \sqrt{(1-2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2 + 2}}$$

$$\omega_{BW} = \frac{\pi}{T_p \sqrt{1-\zeta^2}} \sqrt{(1-2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2 + 2}}$$

$\omega_{BW}$  = frequency at which magnitude is 3dB down

from value at dc (0 rad/sec), or  $M = \frac{1}{\sqrt{2}}$  .

# Find $\omega_{BW}$ from Open-loop Frequency Response



**From open-loop frequency response, we can find  $\omega_{BW}$  at the open-loop frequency that the magnitude lies between -6dB to -7.5dB (phase between -135 to -225)**

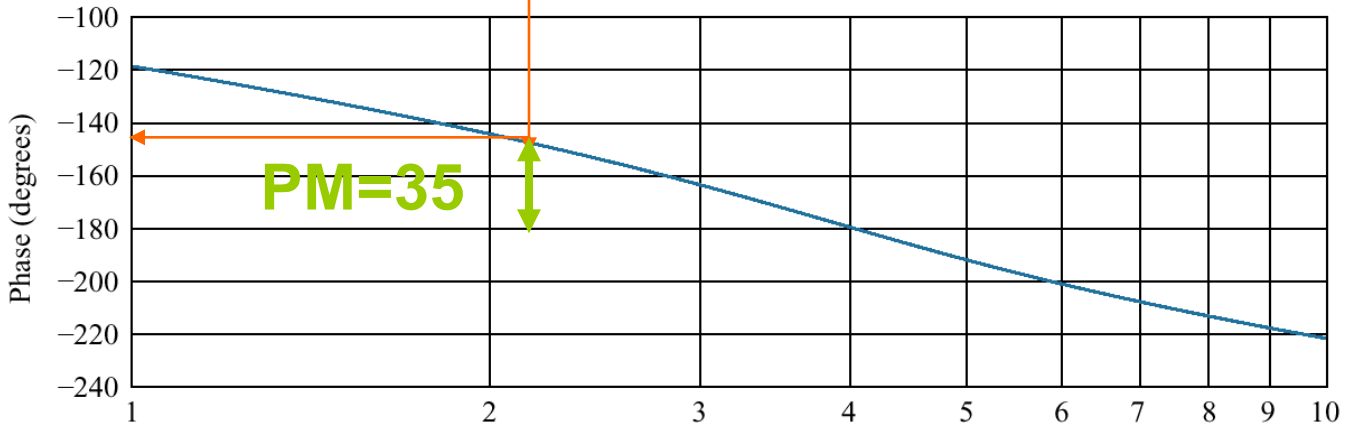
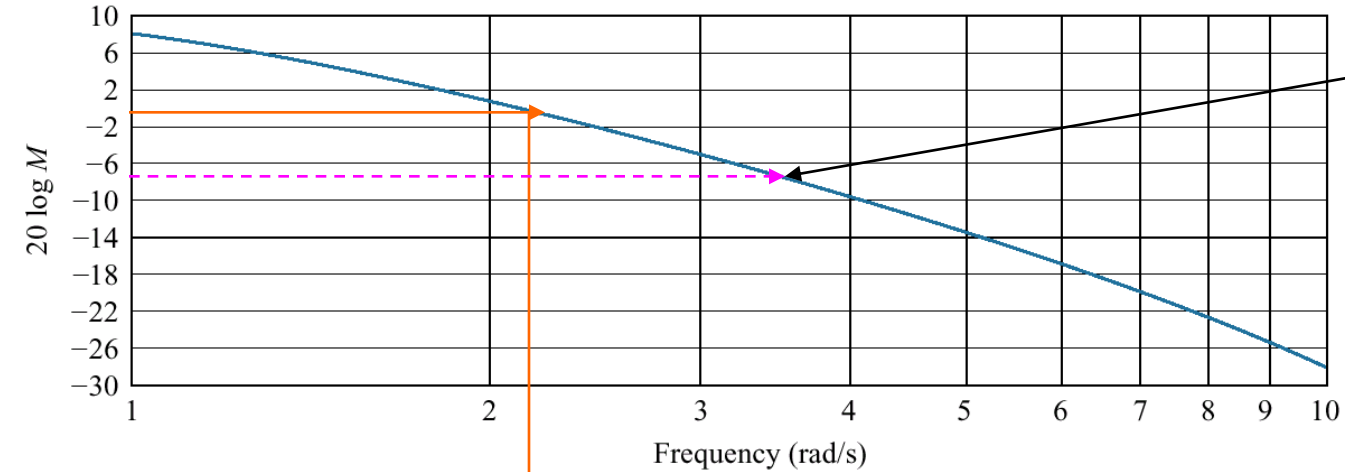
# Relationship between damping ratio and phase margin of open-loop frequency response

**Phase margin of open-loop frequency response  
Can be written in terms of damping ratio as following**

$$\phi_M = \tan^{-1} \frac{2\zeta}{\sqrt{-2\zeta^2 + \sqrt{1 + 4\zeta^4}}}$$

# Example

Open-loop system with a unity feedback has a bode plot below, approximate settling time and peak time



$$\phi_M = \tan^{-1} \frac{2\zeta}{\sqrt{-2\zeta^2 + \sqrt{1+4\zeta^4}}}$$

**Solve for PM = 35**    $\zeta = 0.32$

$$T_s = \frac{4}{\omega_{BW} \zeta} \sqrt{(1-2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2 + 2}}$$
$$= 5.5$$

$$T_p = \frac{\pi}{\omega_{BW} \sqrt{1-\zeta^2}} \sqrt{(1-2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2 + 2}}$$
$$= 1.43$$