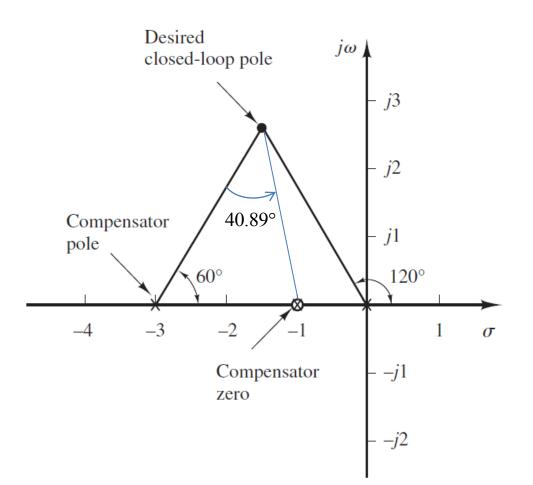
If static error constants are not specified, determine the location of the pole and zero of the lead compensator so that the lead compensator will contribute the necessary angle.



Step-5 (Example-1)

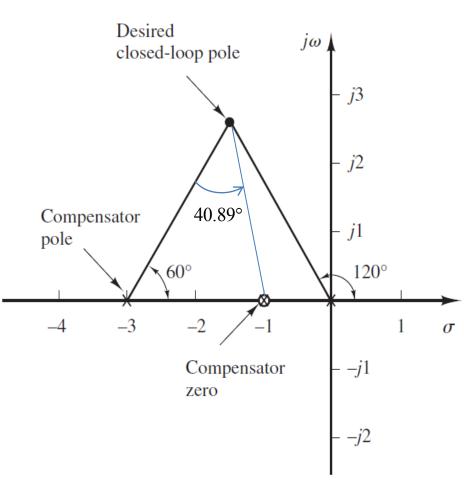
• The pole and zero of compensator are determined as

$$G_c(s) = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}} = K_c \frac{s + 1}{s + 3}$$

The Value of *α* can be determined as

$$\frac{1}{T} = 1 \xrightarrow{\text{yields}} T = 1$$

 $\frac{1}{\alpha T} = 3 \xrightarrow{\text{yields}} \alpha = 0.333$



Solution-1

Step-6 (Example-1)

Solution-1

The Value of K_c can be determined using magnitude condition.

$$\begin{vmatrix} K_c \frac{(s+1)}{s+3} \frac{10}{s(s+1)} \end{vmatrix}_{s=-1.5+j2.5981} = 1$$

$$\begin{vmatrix} K_c \frac{10}{s(s+3)} \end{vmatrix}_{s=-1.5+j2.5981} = 1$$

$$K_c = \left| \frac{s(s+3)}{10} \right|_{s=-1.5+j2.5981} = 0.9$$

$$G_c(s) = 0.9 \frac{s+1}{s+3}$$

Desired

Solution-1

Final Design Check

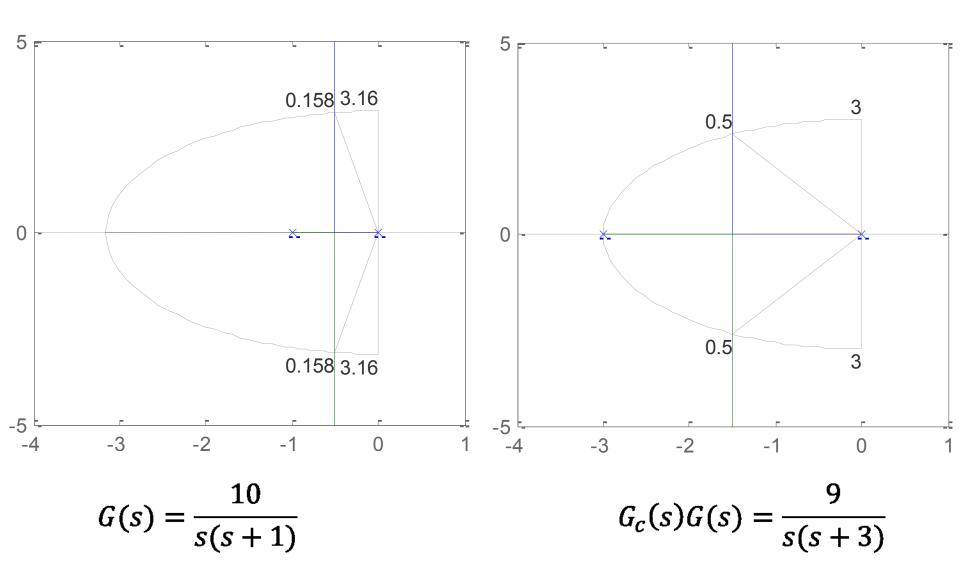
• The open loop transfer function of the designed system then becomes

$$G_c(s)G(s) = \frac{9}{s(s+3)}$$

• The closed loop transfer function of compensated system becomes.

$$\frac{C(s)}{R(s)} = \frac{9}{s^2 + 3s + 9}$$

Final Design Check Solution-1



Solution-1

Final Design Check

• The static velocity error constant for original system is obtained as follows.

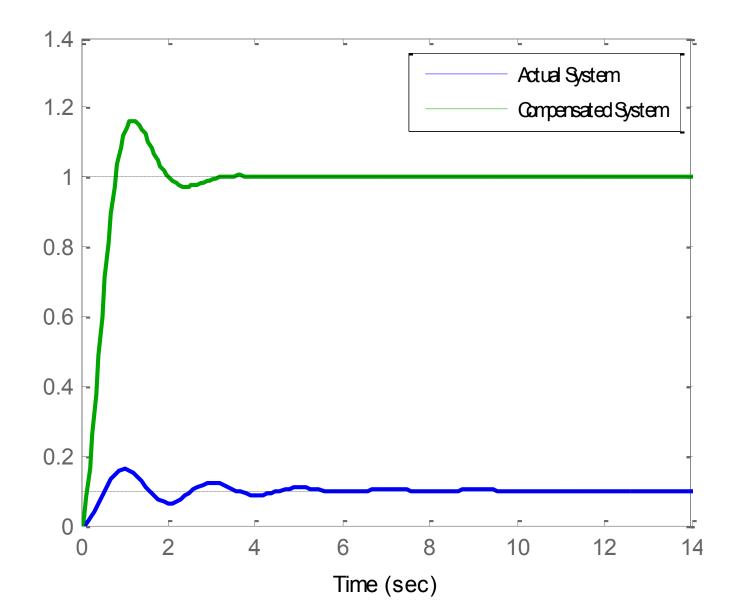
$$K_{\nu} = \lim_{s \to 0} sG(s)$$
$$K_{\nu} = \lim_{s \to 0} s\left[\frac{10}{s(s+1)}\right] = 10$$

• The steady state error is then calculated as

$$e_{ss} = \frac{1}{K_{\nu}} = \frac{1}{10} = 0.1$$

Final Design Check





Solution-1

Final Design Check

• The static velocity error constant for the compensated system can be calculated as

$$K_{\nu} = \lim_{s \to 0} sG_c(s)G(s)$$
$$K_{\nu} = \lim_{s \to 0} s\left[\frac{9}{s(s+3)}\right] = 3$$

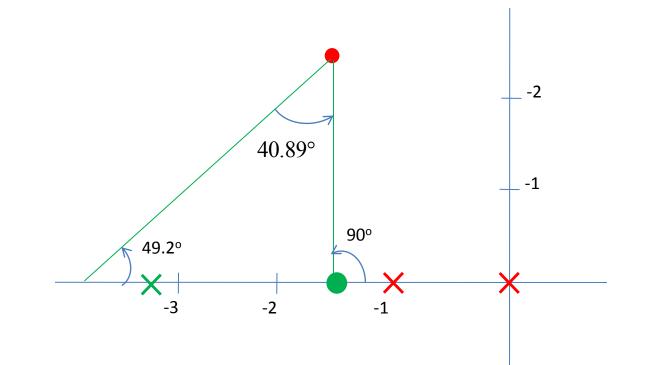
• The steady state error is then calculated as

$$e_{ss} = \frac{1}{K_v} = \frac{1}{3} = 0.333$$

Step-5 (Exampl-1)

Solution-2

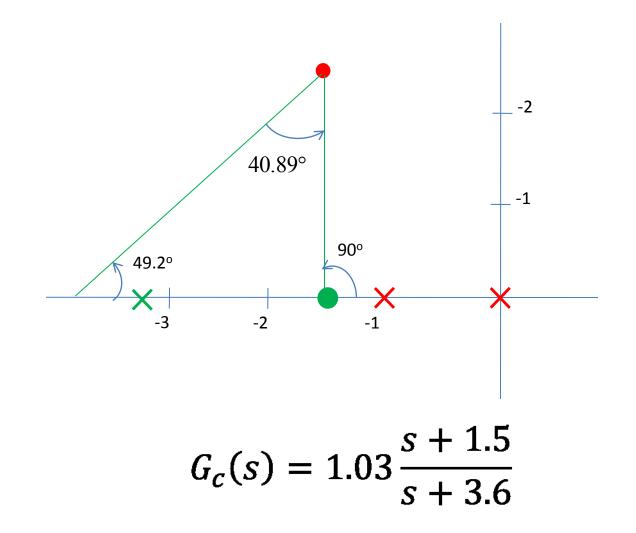
• Solution-2



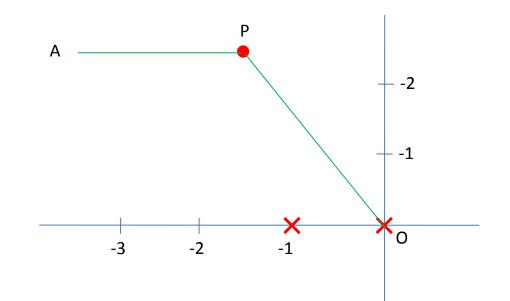
Solution-2

Step-5 (Exampl-1)

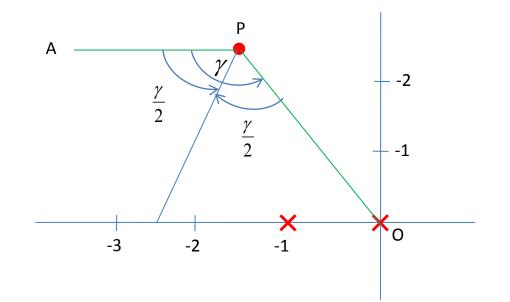
• Solution-2



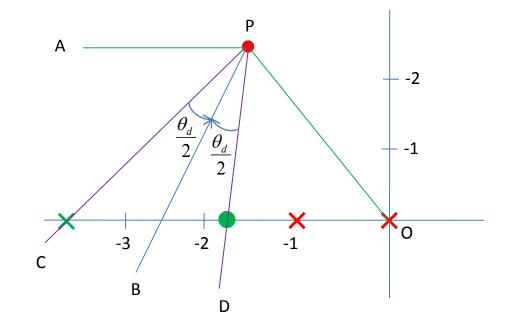
- If no other requirements are imposed on the system, try to make the value of α as large as possible. A larger value of α generally results in a larger value of K, which is desirable.
- Procedure to obtain a largest possible value for α .
 - First, draw a horizontal line passing through point *P*, the desired location for one of the dominant closed-loop poles. This is shown as line PA in following figure.
 - Draw also a line connecting point P and the origin O.



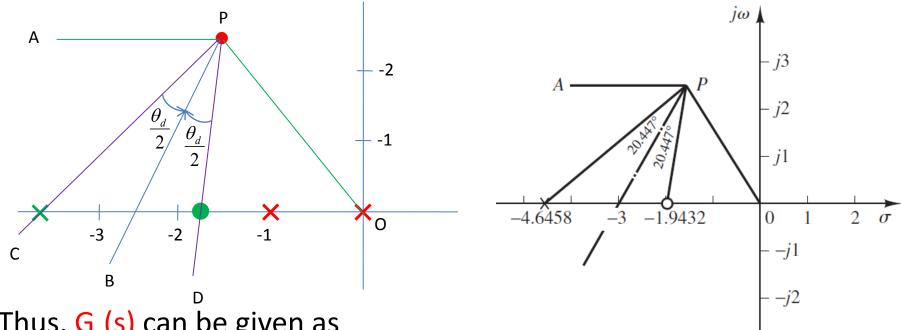
• Bisect the angle between the lines PA and PO, as shown in following figure.



- Draw two lines PC and PD that make angles $\pm \frac{\theta_d}{2}$ with the the bisector PB.
- The intersections of PC and PD with the negative real axis give the necessary locations for the pole and zero of the lead network.



The lead compensator has zero at s=-1.9432 and pole at s=-4.6458.



Thus, G_c(s) can be given as

$$G_c(s) = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}} = K_c \frac{s + 1.9432}{s + 4.6458}$$

Step-5 (Example-1)

Solution-3

$$G_c(s) = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}} = K_c \frac{s + 1.9432}{s + 4.6458}$$

• For this compensator value of α is

$$\frac{1}{T} = 1.9432 \xrightarrow{\text{yields}} T = 0.514$$

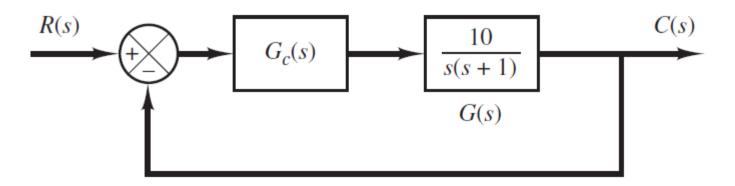
Also

$$\frac{1}{\alpha T} = 4.6458 \xrightarrow{\text{yields}} \alpha = 0.418$$

Step-6 (Example-1)

Solution-3

- Determine the value of K_c of the lead compensator from the magnitude condition.



$$G(s)G_c(s)H(s) = \frac{10K_c(s+1.9432)}{s(s+1)(s+4.6458)}$$

$$\left|\frac{10K_c(s+1.9432)}{s(s+1)(s+4.6458)}\right|_{s=-1.5+j2.5981} = 1$$

Step-6 (Example-1)

Solution-3

• The K_c is calculated as

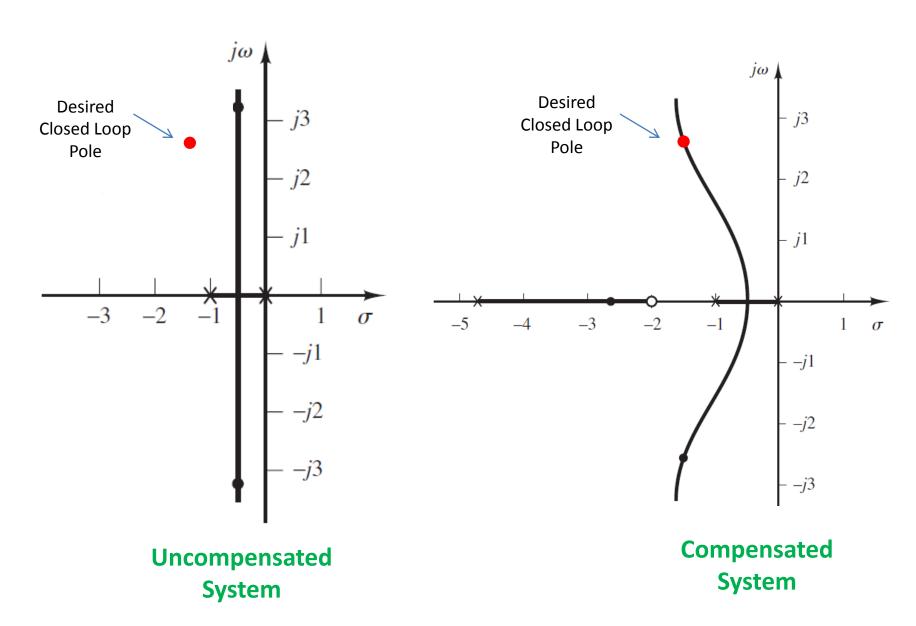
$$K_c = 1.2287$$

 Hence, the lead compensator G_c(s) just designed is given by

$$G_c(s) = 1.2287 \frac{s + 1.9432}{s + 4.6458}$$

Final Design Check

Solution-3



Final Design Check Solution-3

 It is worthwhile to check the static velocity error constant K, for the system just designed.

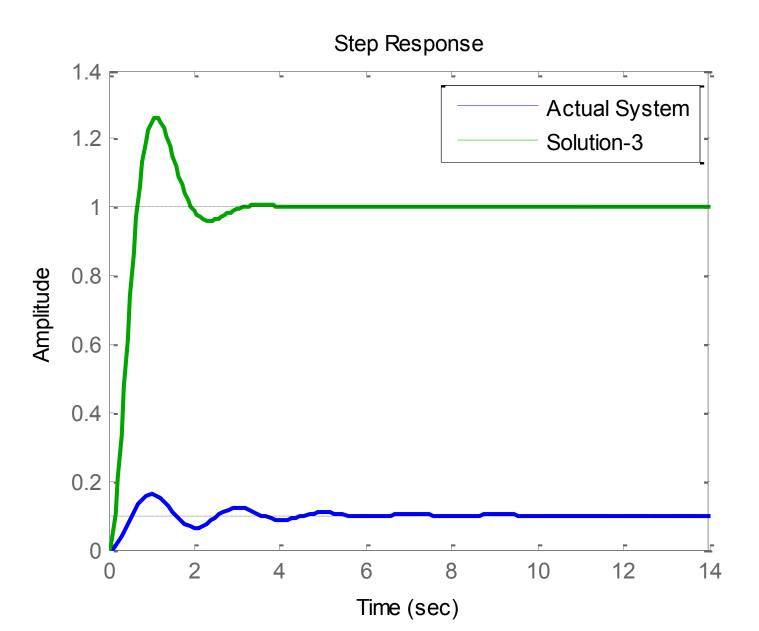
$$K_{v} = \lim_{s \to 0} sG_{c}(s)G(s)$$

$$K_{\nu} = \lim_{s \to 0} s \left[1.2287 \frac{s + 1.9432}{s + 4.6458} \frac{10}{s(s+1)} \right] = 5.139$$

• Steady state error is

$$e_{ss} = \frac{1}{K_{v}} = \frac{1}{5.139} = 0.194$$

Final Design Check

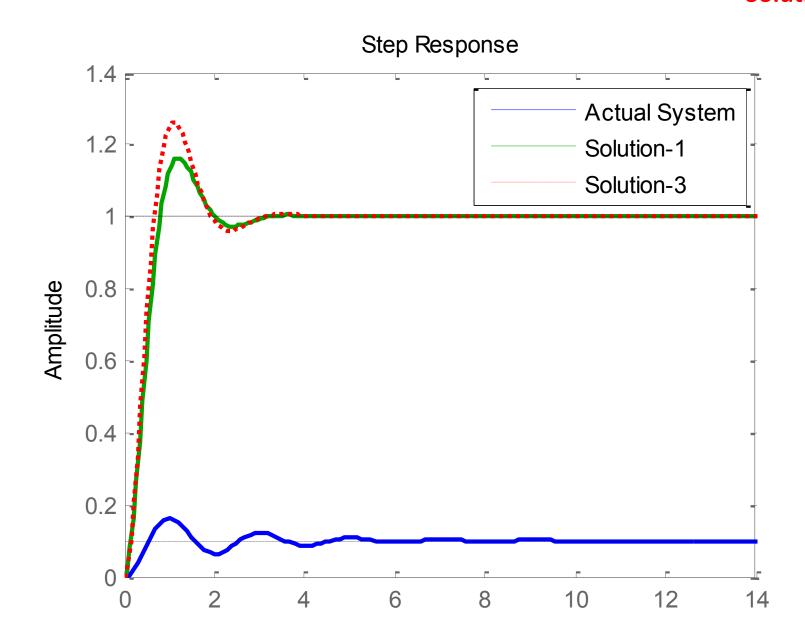


Solution-3

Final Design Check

Solution-3

Solution-1



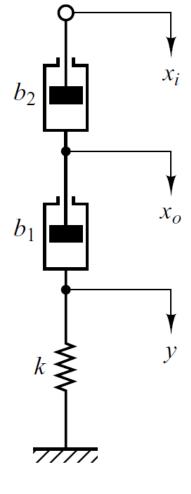
Mechanical Lead Compensator

- Figure shows the mechanical lead compensator.
- Equations are obtained as

$$b_2(\dot{x}_i - \dot{x}_o) = b_1(\dot{x}_o - \dot{y})$$
$$b_1(\dot{x}_o - \dot{y}) = ky$$

 Taking Laplace transform of these equation assuming zero initial conditions and eliminatin Y(s), we obtain

$$\frac{X_o(s)}{X_i(s)} = \frac{b_2}{b_1 + b_2} \frac{\frac{b_1}{k}s + 1}{\frac{b_2}{b_1 + b_2}\frac{b_1}{k}s + 1}$$



Mechanical Lead Compensator

$$\frac{X_o(s)}{X_i(s)} = \frac{b_2}{b_1 + b_2} \frac{\frac{b_1}{k}s + 1}{\frac{b_2}{b_1 + b_2}\frac{b_1}{k}s + 1}$$

• By defining

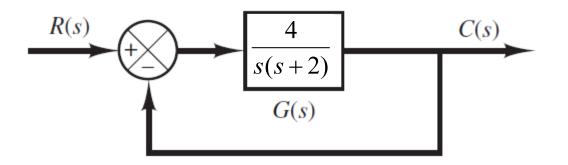
$$\frac{b_1}{k}=T, \qquad \frac{b_2}{b_1+b_2}=\alpha<1$$

• We obtain

$$\frac{X_o(s)}{X_i(s)} = \alpha \frac{Ts+1}{\alpha Ts+1} = \frac{s+\frac{1}{T}}{s+\frac{1}{\alpha T}}$$

Exampl-2

• Design a mechanical lead compensator for following system.



 The damping ratio of closed loop poles is 0.5 and natural undamped frequency 2 rad/sec. It is desired to modify the closed loop poles so that natural undamped frequency becomes 4 rad/sec without changing the damping ratio.

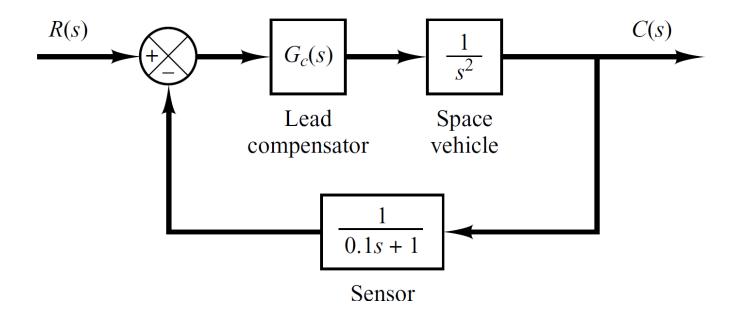
Electrical Lead Compensator R1 $V_i(s)$ $V_i(s)$ $V_i(s)$ $V_i(s)$ $V_i(s)$ $V_i(s)$

$$\frac{V_o(s)}{V_i(s)}_c = \frac{R_2}{R_1 + R_2} \frac{R_1 C s + 1}{\frac{R_1 R_2}{R_1 + R_2} C s + 1}$$

$$T = R_1 C$$
 $aT = \frac{R_1 R_2 C}{R_1 + R_2}$ $a = \frac{R_2}{R_1 + R_2}$ $K_c = 1$

Example-3

• Consider the model of space vehicle control system depicted in following figure.



 Design an Electrical lead compensator such that the damping ratio and natural undamped frequency of dominant closed loop poles are 0.5 and 2 rad/sec.