

Aperture Antennas

• Aperture antennas (horns and reflectors) have a physical collecting area that can be easily calculated from their dimensions: D^2

from their dimensions:
$$A_{phy} = \pi r^2 = \pi \frac{D^2}{4}$$

• Therefore, using Eqn. 4.7 and Eqn. 4.5 we can obtain the formula for aperture antenna gain as:

$$Gain = \frac{4\pi A_e}{\lambda^2} = \frac{4\pi A_{phy}}{\lambda^2} \times \eta$$

$$Gain = \left(\frac{\pi D}{\lambda}\right)^2 \times \eta$$

Typical values of η :

-Reflectors: 50-60%

-Horns: 65-80 %



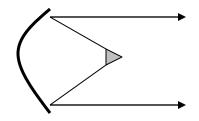
<u> Aperture Antenna Types</u>

- HORN
 - Efficient, Low Gain, Wide Beam
- REFLECTOR
 - High Gain, Narrow Beam, May have to be deployed in space

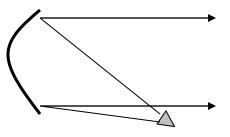
Let's concentrate on the *REFLECTORS* in the next slides



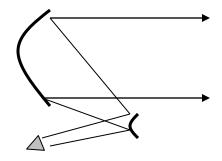
Reflector Types



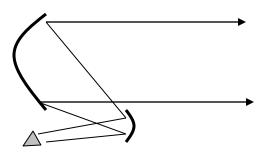
Symmetrical, Front-Fed



Offset, Front-Fed



Offset-Fed, Cassegranian



Offset-Fed, Gregorian

<u>Reflector Antenna - 1</u>

• A rule of thumb to calculate a reflector **antenna beamwidth** in a given plane as a function of the antenna dimension in that plane is given by:

$$\theta_{3dB} \cong \frac{75\lambda}{D}$$
 degrees (Eqn. 3.2)

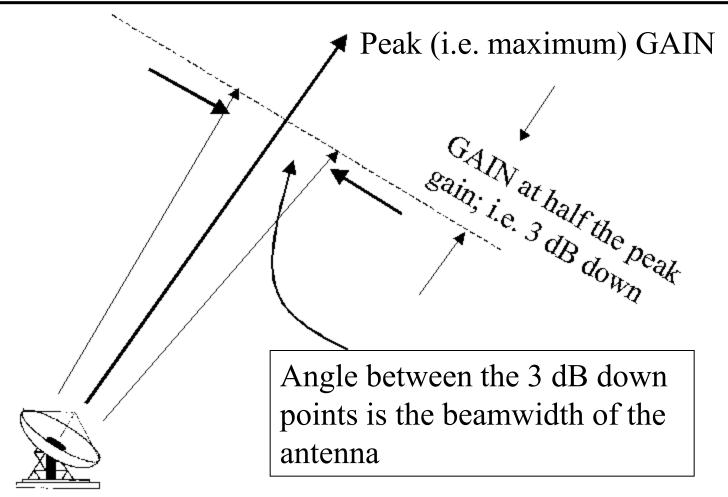
• The approximation above, together with the definition of gain (previous page) allow a gain approximation (for reflectors only):

$$Gain \cong \eta \left(\frac{75\pi}{\theta_{3dB}}\right)^2 = \eta \frac{(75\pi)^2}{\theta_{3dBH}\theta_{3dBE}}$$

• Assuming for instance a typical aperture efficiency of 0.55 gives:

$$Gain \cong \frac{30,000}{(\theta_{3dB})^2} = \frac{30,000}{\theta_{3dBH}\theta_{3dBE}}$$

Antenna Beamwidth



Back to Received Power...

The power available to a receive antenna of effective area $A_r = A_e$ m² is:

$$P_r = F \times A_r = \frac{P_t G_t A_e}{4\pi R^2}$$
 (Eqn. 4.6)

Where A_r = receive antenna effective aperture area = A_e

• Inverting the equation given for gain (Eq. 4.7) gives:

$$G_r = \frac{4\pi A_e}{\lambda^2} \qquad \text{Inverting...} \qquad A_e = \frac{G_r \lambda^2}{4\pi}$$

Back to Received Power...

• Substituting in Eqn. 4.6 gives:

$$P_r = P_t G_t G_r \left(\frac{\lambda}{4\pi R}\right)^2$$
 Friis Transmission Formula (Eqn. 4.8)

• The inverse of the term at the right referred to as "Path Loss", also known as "Free Space Loss" (Lp):

$$L_p = \left(\frac{4\pi R}{\lambda}\right)^2 \qquad \text{Therefore...} \qquad P_r = \frac{P_t G_t G_r}{L_p}$$

More complete formulation

- Demonstrated formula assumes idealized case.
- Free Space Loss (Lp) represents spherical spreading only.
- Other effects need to be accounted for in the transmission equation:
 - $L_a = Losses$ due to attenuation in atmosphere
 - \mathbf{L}_{ta} = Losses associated with transmitting antenna
 - L_{ra} = Losses associates with receiving antenna
 - $L_{pol} = Losses$ due to polarization mismatch
 - \mathbf{E} $\mathbf{L}_{\text{other}}$ = (any other known loss as much detail as available)
 - Lr = additional Losses at receiver (after receiving antenna)

$$P_{r} = \frac{P_{t}G_{t}G_{r}}{L_{p}L_{a}L_{ta}L_{ra}L_{pol}L_{other}L_{r}}$$

Transmission Formula

Some intermediate variables were also defined before:

$$P_t = P_{out}/L_t$$
 $EIRP = P_t G_t$ Where:

- P_t = Power into antenna
- L_t = Loss between power source and antenna
- EIRP = effective isotropic radiated power

•Therefore, there are many ways the formula could be rewritten. The user has to pick the one most suitable to each need.

$$P_{r} = \frac{P_{t}G_{t}G_{r}}{L_{p}L_{a}L_{ta}L_{ra}L_{pol}L_{other}L_{r}}$$

$$= \frac{EIRP \times G_{r}}{L_{p}L_{a}L_{ta}L_{ra}L_{pol}L_{other}L_{r}}$$

$$= \frac{P_{out}G_{t}G_{r}}{L_{t}L_{p}L_{a}L_{ta}L_{ta}L_{pol}L_{other}L_{r}}$$

Link Power Budget

Tx EIRP

Transmission:

HPA Power
Transmission Losses
(cables & connectors)
Antenna Gain

Antenna Pointing Loss
Free Space Loss
Atmospheric Loss
(gaseous, clouds, rain)
Rx Antenna Pointing Loss

Reception:

Antenna gain
Reception Losses
(cables & connectors)
Noise Temperature
Contribution

Rx





Why dB?

- There is a large dynamic range of parameters in satellite communications
 - A typical satellite antenna has a gain of >500
 - Received power flux is about one part in 100,000,000,000,000,000

 That's a lot of zeros! of the transmitted power
- Wouldn't it be nice to have a better way to write these large numbers?
- dB also lets many calculations be addition or subtraction!

What is a dB?

- Decibel (dB) is the unit for 10 times the base 10 logarithmic ratio of two powers
- For instance: gain is defined as P_{out}/P_{in}

• in dB:
$$G = 10 \cdot \log \left(\frac{P_{out}}{P_{in}} \right) dB$$

(where P_{out} is usually greater than P_{in})

on the interval of the in

A Dangerous Calculation in dB!

dB ratios must <u>NEVER</u> be calculated as 20 times the base 10 logarithmic ratio of voltages

Unless of course its more convenient, in which case you must be very, very careful. Here's why these calculations are performed for say a (passive)

$$P_{in} = \frac{V_{in}^2}{R_{in}} \qquad P_{out} = \frac{V_{out}^2}{R_{out}}$$

$$G = 10 \log \left(\frac{P_{out}}{P_{in}}\right) = 10 \log \left(\frac{\frac{V_{out}^2}{R_{out}}}{\frac{V_{in}^2}{R_{in}}}\right)$$

transformer with winding ratios of 4 output turns per input turn, $V_{out} = 4$ when $V_{in} = 1$. If the last term is neglected, the gain appears to be $G = 20\log(4) = 12$ dB. This is a curious result for a passive device! If the last term is used, $R_{out} = 16$ for $R_{in} = 1$, so the last term is -12 dB. This restores the balance at G = 0 as expected for an ideal passive device.

This term is usually forgotten (with tragic results!)

$$G = 10\log\left(\frac{V_{out}^2}{V_{in}^2}\right) + 10\log\left(\frac{R_{in}}{R_{out}}\right) = 20\log\left(\frac{V_{out}}{V_{in}}\right) + 10\log\left(\frac{R_{in}}{R_{out}}\right)$$

Using Decibels - 1

Rules:

Multiply A x B: (Add dB values)

•Divide A / B:

(Subtract dB values)

$$10\log_{10}(A \times B)$$

$$= 10\log_{10}(A) + 10\log_{10}(B)$$

$$= AdB + BdB$$

$$= (A + B)dB$$

$$10\log_{10}(A/B)$$

$$=10\log_{10}(A)-10\log_{10}(B)$$

$$=AdB-BdB$$

$$=(A-B)dB$$