Each of three-phase generators can be connected to one of three identical loads.

This way the system would consist of three single-phase circuits differing in phase angle by 120^o.

The current flowing to each load can be found as

$$I = \frac{V}{Z}$$



Therefore, the currents flowing in each phase are



$$I_{A} = \frac{V \angle 0^{0}}{Z \angle \theta} = I \angle -\theta$$

$$I_{B} = \frac{V \angle -120^{0}}{Z \angle \theta} = I \angle -120 - \theta$$

$$I_{A} = \frac{V \angle -240^{0}}{Z \angle \theta} = I \angle -240 - \theta$$

The current flowing through a neutral can be found as

 $I_N = I_A + I_B + I_C = I \angle -\theta + I \angle -\theta - 120^0 + I \angle -\theta - 240^0$

 $= I \cos(-\theta) + jI \sin(-\theta) + I \cos(-\theta - 120^{\circ}) + jI \sin(-\theta - 120^{\circ}) + I \cos(-\theta - 240^{\circ}) + jI \sin(-\theta - 240^{\circ})$ $= I \Big[\cos(-\theta) + \cos(-\theta - 120^{\circ}) + \cos(-\theta - 240^{\circ}) \Big] + jI \Big[\sin(-\theta) + \sin(-\theta - 120^{\circ}) + \sin(-\theta - 240^{\circ}) \Big]$ $= I \Big[\cos(-\theta) + \cos(-\theta) \cos(120^{\circ}) + \sin(-\theta) \sin(120^{\circ}) + \cos(-\theta) \cos(240^{\circ}) + \sin(-\theta) \sin(240^{\circ}) \Big]$ $+ jI \Big[\sin(-\theta) + \sin(-\theta) \cos(120^{\circ}) - \cos(-\theta) \sin(120^{\circ}) + \sin(-\theta) \cos(240^{\circ}) - \cos(-\theta) \sin(240^{\circ}) \Big]$

Which is:
$$I_{N} = I \left[\cos(-\theta) - \frac{1}{2}\cos(-\theta) + \frac{\sqrt{3}}{2}\sin(-\theta) - \frac{1}{2}\cos(-\theta) - \frac{\sqrt{3}}{2}\sin(-\theta) \right]$$
$$+ jI \left[\sin(-\theta) - \frac{1}{2}\sin(-\theta) + \frac{\sqrt{3}}{2}\cos(-\theta) - \frac{1}{2}\sin(-\theta) - \frac{\sqrt{3}}{2}\cos(-\theta) \right]$$
$$= 0$$

As long as the three loads are equal, the return current in the neutral is zero!

Such three-phase power systems (equal magnitude, phase differences of 120⁰, identical loads) are called balanced.

In a balanced system, the neutral is unnecessary!

Phase Sequence is the order in which the voltages in the individual phases peak.



There are two types of connections in three-phase circuits: Y and Δ .



Each generator and each load can be either Y- or Δ -connected. Any number of Y- and Δ -connected elements may be mixed in a power system.

Phase quantities - voltages and currents in a given phase. Line quantities – voltages between the lines and currents in the lines connected to the generators.

Y-connection

Assuming a resistive load...



Y-connection (cont)

 $V_{an} = V_{\phi} \angle 0^{0}$ $V_{bn} = V_{\phi} \angle -120^{0}$ $V_{cn} = V_{\phi} \angle -240^{0}$

Since we assume a resistive load:

 $I_a = I_{\phi} \angle 0^0$ $I_b = I_{\phi} \angle -120^0$ $I_c = I_{\phi} \angle -240^0$

Y-connection (cont. 2)

The current in any line is the same as the current in the corresponding phase.

$$I_L = I_{\phi}$$

Voltages are:

$$V_{ab} = V_a - V_b = V_{\phi} \angle 0^0 - V_{\phi} \angle -120^0 = V_{\phi} - \left(-\frac{1}{2}V_{\phi} - j\frac{\sqrt{3}}{2}V_{\phi}\right) = \frac{3}{2}V_{\phi} + j\frac{\sqrt{3}}{2}V_{\phi}$$
$$= \sqrt{3}V_{\phi}\left(\frac{\sqrt{3}}{2} + j\frac{1}{2}\right) = \sqrt{3}V_{\phi} \angle 30^0$$

Y-connection (cont. 3)

Magnitudes of the line-to-line voltages and the line-to-neutral voltages are related as:

$$V_{LL} = \sqrt{3}V_{\phi}$$

In addition, the line voltages are shifted by 30^o with respect to the phase voltages.

In a connection with *abc* sequence, the voltage of a line **leads** the phase voltage.



Δ -connection

assuming a resistive load:



 $V_{ab} = V_{\phi} \angle 0^{0}$ $V_{bc} = V_{\phi} \angle -120^{0}$ $V_{ca} = V_{\phi} \angle -240^{0}$

(3.14.1)

 $I_{ab} = I_{\phi} \angle 0^{0}$ $I_{bc} = I_{\phi} \angle -120^{0}$ $I_{ca} = I_{\phi} \angle -240^{0}$

 Δ -connection (cont.)

$$V_{LL} = V_{\phi}$$

The currents are:

$$I_{a} = I_{ab} - I_{ca} = I_{\phi} \angle 0^{0} - I_{\phi} \angle 240^{0} = I_{\phi} - \left(-\frac{1}{2}I_{\phi} + j\frac{\sqrt{3}}{2}I_{\phi}\right)$$
$$= \frac{3}{2}I_{\phi} - j\frac{\sqrt{3}}{2}I_{\phi} = \sqrt{3}I_{\phi}\left(\frac{\sqrt{3}}{2} - j\frac{1}{2}\right) = \sqrt{3}I_{\phi} \angle -30^{0}$$
The magnitudes:
$$I_{L} = \sqrt{3}I_{\phi}$$

For the connections with the *abc* phase sequences, the current of a line **lags** the corresponding phase current by 30^o (see Figure below).



For the connections with the *acb* phase sequences, the line current **leads** the corresponding phase current by 30⁰.

For a balanced Y-connected load with the impedance $Z_{\phi} = Z \angle \theta^0$:

and voltages: $v_{an}(t) = \sqrt{2}V \sin \omega t$ $v_{bn}(t) = \sqrt{2}V \sin(\omega t - 120^{\circ})$ $v_{cn}(t) = \sqrt{2}V \sin(\omega t - 240^{\circ})$ (3.17.2)

The currents can be found:

 $i_{a}(t) = \sqrt{2}I\sin(\omega t - \theta)$ $i_{b}(t) = \sqrt{2}I\sin(\omega t - 120^{0} - \theta)$ $i_{c}(t) = \sqrt{2}I\sin(\omega t - 240^{0} - \theta) \quad (3.17.2)$



The instantaneous power is:

p(t) = v(t)i(t)

Therefore, the instantaneous power supplied to each phase is:

 $p_{a}(t) = v_{an}(t)i_{a}(t) = 2VI\sin(\omega t)\sin(\omega t - \theta)$ $p_{b}(t) = v_{bn}(t)i_{b}(t) = 2VI\sin(\omega t - 120^{0})\sin(\omega t - 120^{0} - \theta)$ $p_{c}(t) = v_{cn}(t)i_{c}(t) = 2VI\sin(\omega t - 240^{0})\sin(\omega t - 240^{0} - \theta)$

Since

$$\sin \alpha \sin \beta = \frac{1}{2} \left[\cos(\alpha - \beta) - \cos(\alpha + \beta) \right]$$

Therefore

$$p_{a}(t) = VI \left[\cos \theta - \cos(2\omega t - \theta) \right]$$
$$p_{b}(t) = VI \left[\cos \theta - \cos(2\omega t - 240^{0} - \theta) \right]$$
$$p_{c}(t) = VI \left[\cos \theta - \cos(2\omega t - 480^{0} - \theta) \right]$$

The total power on the load

 $p_{tot}(t) = p_a(t) + p_b(t) + p_c(t) = 3VI \cos \theta$

The pulsing components cancel each other because of 120° phase shifts.

The instantaneous power in phases.

The total power supplied to the load is constant.



Phase quantities in each phase of a Y- or Δ -connection.

Real $P = 3V_{\phi}I_{\phi}\cos\theta = 3I_{\phi}^{2}Z\cos\theta$ Reactive $Q = 3V_{\phi}I_{\phi}\sin\theta = 3I_{\phi}^{2}Z\sin\theta$ Apparent $S = 3V_{\phi}I_{\phi} = 3I_{\phi}^{2}Z$

Note: these equations are valid for balanced loads only.

Line quantities: Y-connection.

Power consumed by a load:

Since for this load

Therefore:

Finally:

$$I_L = I_{\phi}$$
 and $V_{LL} = \sqrt{3}V_{\phi}$

$$P = 3\frac{V_{LL}}{\sqrt{3}}I_L\cos\theta$$

 $P = 3V_{\phi}I_{\phi}\cos\theta$

$$P = \sqrt{3} V_{LL} I_L \cos \theta$$

Note: these equations are valid for balanced loads only.

Line quantities: Δ -connection.

Power consumed by a load:

Since for this load

Therefore:

Finally:

$$I_{L} = \sqrt{3}I_{\phi} \text{ and } V_{LL} = V_{\phi}$$
$$P = 3\frac{I_{L}}{\sqrt{3}}V_{LL}\cos\theta$$

$$P = \sqrt{3} V_{LL} I_L \cos \theta$$

 $P = 3V_{\phi}I_{\phi}\cos\theta$

Same as for a Y-connected load!

Note: these equations were derived for a balanced load.

Line quantities: Y- and Δ -connection.

Reactive power

$$Q = \sqrt{3} V_{LL} I_L \sin \theta$$

Apparent power

$$S = \sqrt{3}V_{LL}I_L$$

Note: θ is the angle between the phase voltage and the phase current – the impedance angle.